CMOS SOCs at 100 GHz: System Architectures, Device Characterization, and IC Design Examples

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Outline

•Why?

•Measured 65nm MOSFETs: are they really that bad (for analog/RF)?

•60-100 GHz circuits in 90nm and 65nm CMOS

Summary







Remote sensing (passive imaging) (E. Laskin et al. RFIC-2007) 80-GHz PLL 160-GHz 160-GHz Receiver Receiver 80-GHz 80-GHz Receiver Receiver

Multiphase/multi-frequency clock distribution

•Quad signals @ 80 GHz. differential at 160 GHz.

Save power by sharing PLL among





80GHz inverse scattering active imager 3-stage IF Low IF: 1MHz-10MHz LNA 80 GHz BUF transceiver array 32 Reference transceiver 2.5 GHz BUF PLL Inhomogeneous VCO PA 80 GHz object to be imaged Switched TX/RX Freq. 2-stage Crosstalk suppression through system architecture Different frequencies in TX and RX modes One transmitter on, all other TXRX in receive mode Need very low power for array integration





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•Why?

•65nm CMOS Device Characterization

•60-100 GHz Circuits in 90nm and 65nm CMOS

Summary









GP and LP 65nm CMOS



•GP 30% faster than LP and 300mV lower V_{GS} => lower power!

•Constant-current-density bias at 0.3-0.4mA/ μ m => robust to I_{DS} variation

•VT variation is large but mostly irrelevant



MOSFET DC gain scaling: think current density!



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- •65nm CMOS Device Characterization
- •60-100 GHz Circuits in 90nm and 65nm CMOS
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90nm CMOS Receiver Measurements



90nm CMOS Receiver Measurements (ii)



60GHz 90nm GP CMOS Upconverter



CMOS Upconverter RF Spectrum

🔆 Agilent 13:27:00 Oct 27, 2006







60GHz PA in 90-nm RFCMOS (T.Yao et al. RFIC-06)



- G=5dB, O_{1dB}=6.4dBm, P_{sat}=9dBm
- PAE=7%
- 14dB gain version in 90nm digital GP CMOS also tested





Sorin Voinigescu, ISCAS-2007 May 29, 2007



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77GHz Colpitts VCO in (digital) 90-nm GP CMOS (K.Tang et al. CSICS-06)



W-band 3-stage cascode LNA in 65nm LP RF-CMOS S. Nicolson (CSICS 2006) $V_{_{DD}}$ $V_{_{DD}}$ $V_{_{DD}}$ Ĺ _{D2} 20x1.5µm $L_{_{D1}}$ 000 000 two-side gate contact $T_{_{D1}}$ $V_{_{GBIAS}}$ V_{casc} of $\mathbf{V}_{\mathrm{casc}}$ V_{casc} $\mathbf{V}_{\mathrm{out}}$ L_M

•Inductive broadbanding (L_{M}) -> also lowers NF₅₀ (CS-CG topologies also fabricated)

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Pad capacitance included in design methodology at mm-waves

V_{GBIAS}

$$R_{in} = Z_0 / [1 + (\omega Z_0 C_{PAD})^2] = R_s + R_g + L_s \omega_T (casc)$$

$$R_{sopt} = Z_0 / [1 + (\omega Z_0 C_{PAD})^2] = R_s + R_g + f_T (casc) / (2fg_m)$$



 $\mathbf{V}_{_{\mathrm{in}}}$

 $T_{_{G}}$

PAD

PAD

000

 L_s

Die photo and measured S-params



•0.4mmx0.4mm including pads

•Overdriven in non-linear mode • S_{11} , S_{22} < -10 dB, S_{12} < -30 dB









Summary

- •CMOS for low-power SOCs up to 100 GHz
- •GP rather than LP CMOS is needed
- •65nm CMOS DC gain is OK
- •We can live with leakage at mm-waves
- •CMOS design based on current density rather than $V_T/V_{eff} =>$ think HBT design
- •60-100 GHz state-of-the-art CMOS circuits in 90nm and 65nm CMOS
- •Temperature and wafer mapping of 60GHz LNA, PA and 90GHz divider show manufacturability of 60-80 GHz radio in nanoscale CMOS
- •SiGe HBT/BiCMOS still higher performance and lower cost than 65nm CMOS





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- •OIT, CFI, ECTI for equipment





60GHz PA Measurements





- Measured S-params on 3 dies
- Peak gain = 5.2dB (60GHz)
- 3-dB BW > 13GHz (52-65GHz)
- S_{22} , S_{11} both matched (60-65GHz)

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$$OP_{1dB} = 6.4dBm, P_{sat} = 9.3dBm$$

• Maximum linearity @ 0.28mA/µm



85-GHz Buffered Colpitts VCO 90-nm GP CMOS











Measured tuning range and output power



Measured 65nm LP MOSFET performance









60-90 GHz Radio Systems

Classical radio architecture: simple and robust at mm-waves Smaller die, lower cost, higher data rate than 2-10 GHz UWB radio

Crucial front-end blocks/issues:





