6.6 A 22.5-to-32Gb/s 3.2pJ/b Referenceless Baud-Rate Digital CDR with DFE and CTLE in 28nm CMOS

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Baud-rate clock and data recovery circuits (CDRs) are becoming more prevalent in high-speed receiver designs as they offer lower power consumption by sampling the received data only once per UI [1,2]. This reduces the number of front-end comparators and clock distribution networks [1]. However, current baud-rate CDRs require an external reference clock [1,2], adding to the system complexity in pin count and clock generation. While frequency detectors (FDs) allow CDR designs to operate without a reference clock and across a wide capture range [3-5], current FDs are not designed for baud-rate CDRs. As well, current FDs rely on sharp data edges and are not designed for significant ISI caused by channel loss at high data rates [3-5]. This work presents a reference-less baudrate CDR that operates from 22.5Gb/s to 32Gb/s with channel loss up to -14.8dB at Nyquist. An FD scheme is proposed that automatically controls an adjustable PD to correct any frequency error. This eliminates the need for a separate frequency acquisition loop in the CDR. The CDR, with a CTLE and a 1-tap DFE, is fabricated in 28nm CMOS. The entire receiver consumes 3.2pJ/b at 32Gb/s PRBS-31.

Figure 6.6.1 illustrates the proposed baud-rate receiver architecture with frequency detection. Full-rate clocking is shown here for conceptual purposes. The incoming waveform is equalized by a CTLE before being sampled at baudrate (i.e. once per UI) by three comparators. Two of the comparators are set to $\pm \alpha$ thresholds to be shared by a 1-tap look-ahead DFE [1]; a third comparator is set to a zero threshold. The outputs of the three comparators form the resulting sample S_n, which is then fed to a pattern filter to be selected if it matches a predefined data sequence. A valid S_n is then used by the proposed FD and the adjustable baud-rate phase detector (PD) in the digital CDR to bring the clock frequency closer to the data rate. Frequency detection operates as follows. Slow/fast clock detectors indicate if there is a frequency error between the recovered clock and incoming data (Slow_{FD} & Fast_{FD}) and feed these indicators to the frequency correction logic where they are accumulated over time. The FD filter then compares the raw accumulated FD output against programmable filter thresholds (± 30 from a range of ± 150). If the high or low thresholds are exceeded, the FD identifies the clock as too slow or too fast, respectively. The FD then digitally adjusts the PD characteristic (PD Adjust Slow/Fast) such that the average PD output corrects for the frequency error over time. If the filter thresholds are not exceeded, the FD allows the PD to operate normally (PD Adjust Normal). An FD lock detector measures the average activity from the slow/fast clock detectors and determines if frequency lock is achieved. This occurs when frequency error falls below ±800ppm, which is within the PD capture range.

The pattern filter and normal PD operation are depicted in Fig. 6.6.2. Similar to [1], both the rising and the falling RX waveforms corresponding to TX data patterns "011" and "100" are considered (however only the rising waveform is shown). From the post-CTLE waveform, three subsequent samples S_{n-1} , S_n , and S_{n+1} are quantized into four distinct voltage "zones". Sequences for which S_{n-1} and S_{n+1} are in Zones 0 and 3, respectively, are identified. Among these sequences, S_n is selected for PD/FD operation only if it falls in Zones 1, 2, or 3; sequences for which S_n lies in Zone 0 are ignored. This ensures the 1-tap look-ahead DFE correctly recovers the "011" data. PD logic is defined by the S_n zone. For normal PD operation, if S_n is in Zones 1 or 2, the recovered clock (CK_{REC}) is early and the PD output (PD_{OUT}) is DN. If S_n is in Zone 3, CK_{REC} is late and PD_{OUT} is UP.

Figure 6.6.3 illustrates the operation of the FD under three cases: normal clock ($f_{CK}=f_{DATA}$), slow clock ($f_{CK}<f_{DATA}$), and fast clock ($f_{CK}>f_{DATA}$). For a normal clock, jitter and CDR dynamics move selected S_n samples about the stable phase lock point, as shown in the 1st row of the table. For this normal PD logic, the average PD characteristic is zero and the PD ensures that the CDR maintains lock for both the VCO frequency and phase. If the recovered clock is slow, the clock drifts with respect to the data, as shown in the 2nd row of the table. As observed on rising waveforms, selected S_n samples drift from Zones 1 to 2 to 3 over time. The slow clock detector in the FD recognizes this and, if it persists, issues a Slow Adjust

signal to the PD. This signal changes the PD characteristic such that the average PD output is positive. Over time, this positive average increases the VCO frequency and corrects the slow clock. A similar procedure is done for a fast clock, as shown in the 3rd row of the table. In all three cases, there exists a stable phase lock point in the PD characteristic. This ensures the CDR automatically phase-locks once FD_{LOCK} is declared. At this point, the PD resumes normal operation.

Figure 6.6.4 presents the receiver schematic for a guarter-rate implementation. The CTLE consists of an adjustable source-degenerated stage followed by a CML buffer to drive ten sampling comparators. The CTLE provides up to 4.0dB gain at 7GHz; this equalizes the channel response up to the first post-cursor ISI for the 1-tap DFE. The ten double-tail comparators operate at guarter-rate to sample the RX waveform once per UI. Of these comparators, eight correspond to the DFE levels $(\pm \alpha)$ for all four clock phases and two correspond to the zero level. While this restricts the S_n samples to be available only at clock phases CK0° and CK180°, it is sufficient for CDR operation and relaxes the CTLE design. A four-stage CML ring VCO operates at quarter-rate ($f_{CK}/4$) to generate the four high-speed quadrature clock phases. The measured VCO tuning range is 5.6-9.0GHz. The demuxed comparator samples are processed by the synthesized digital back-end operating at f_{CK}/32 (CK_{CORF}) from 703.1MHz to 1.125GHz. Within the digital backend, the digital loop filter of the CDR generates coarse and fine codes to control a 10b segmented current DAC. The fine DAC is designed to span 2 LSBs of the coarse DAC. The current DAC achieves a resolution of 3.0MHz/LSB through an Ito-V conversion.

A CDR prototype is fabricated in TSMC 28nm CMOS technology and consumes 65.2-102.0mW when operating from 22.5-32Gb/s respectively (without I/O buffers). Figure 6.6.5 summarizes the measurement results. FD operation is verified by open-loop response and closed-loop capture range measurements. For the open-loop FD response, frequency error $(f_{FBB}=[f_{DATA}-f_{CK}]/f_{CK})$ is measured by forcing the VCO in open loop to 7.0GHz (f_{CK} =28GHz) and transmitting 22.5-32Gb/s PRBS-31 data over a 5" Tyco channel with Nyquist loss ranging from -10.1dB to -14.8dB. The maximum data rate (fDATA) of the measurement equipment is limited to 32Gb/s, corresponding to f_{ERR} ≤+14.3% (interval A in Fig. 6.6.5 openloop measurements). To characterize for f_{ERR} >14.3% (interval B), f_{DATA} is held constant at 32Gb/s and $f_{\mbox{\tiny CK}}$ is reduced. Closed-loop capture range is measured by initializing the VCO in closed-loop to 7.0GHz (f_{cx}=28GHz) and observing the widest range of data rates for which the CDR acquires lock. The CDR locks down to 22.5Gb/s and up to 32Gb/s when no TX jitter is applied, achieving a capture range of 9.5Gb/s (34%). The capture range is limited by the VCO lower limit and the equipment data rate upper limit. Applying 0.2UI_{PP} TX SJ reduces capture range to 25%. The FD improves CDR capture range by up to 227×. Jitter tolerance measurements are shown with the FD enabled and disabled. A real-time oscilloscope measures a maximum FD lock time of 10.1ms for FD_{LOCK}.

Figure 6.6.6 compares the performance of this work against prior work. The entire receiver, including equalizers, competes favourably in terms of power efficiency against prior works with no equalization. Figure 6.6.7 shows the die micrograph.

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Figure 6.6.5: Measurement results: open-loop FD response; CDR capture range vs. TX SJ at 200 MHz; CDR JTOL for 28Gb/s PRBS-31; and lock time vs. freq. error (w/ and w/o $0.2UI_{PP}$ TX SJ at 200 MHz).







Figure 6.6.4: Schematic of complete baud-rate receiver. Baud-rate sampling is implemented with four phases of a quarter-rate clock.

\succ	ISSCC 2014 [3]	ISSCC 2014 [4]	JSCC 2015 [5]	This work
Technology	65nm CMOS	0.18µm BiCMOS	65nm CMOS	28nm CMOS
Supply Voltage	1.2/1.0	1.8	N/A	0.9
Baud-rate?	No	No	No	Yes
Data rate (Gb/s)	4-10.5 (Δ = 6.5)	8.2-10.3 (Δ = 2.1)	8.5-12.1 (Δ = 3.6)	22.5-32* (Δ = 9.5)
Capture Range	65%	21%	36%	34%
Channel Loss (dB)	None reported	None reported	7.0	14.8
Equalization	None	None	None	CTLE + 1-tap DFE
Total Power	22.5	174	43.0	102.0
(mW)	@ 10Gb/s	@ 10.3Gb/s	@ 12.1Gb/s	@ 32Gb/s
FoM (pJ/b)	2.25	16.89	3.55	3.19

*Equipment limit (maximum data rate = 32Gb/s)

Figure 6.6.6: Performance comparison.

