A Passive Filter Aided Timing Recovery Scheme

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Outline

- Introduction
- Baud-rate timing recovery (TR) schemes
- Passive filter
- Measurement Results
- Conclusions



Introduction



Introduction



Introduction

- Why baud-rate over edge-sampled?
- 1. Reduced clock sampling phases results in less power in the VCO and phase detector.
- 2. Better performance in the presence of ISI and random noise.

[F. Musa and A. Chan Carusone,``Modeling and Design of Multilevel Bang-bang CDRs in the Presence of ISI and Noise," *IEEE Transactions on Circuits and Systems I: Regular Papers*, Vol. 54, No. 10, October 2007.]



- Baud-rate architectures for serial links:
- 1. Integrating front-end based clock recovery
- 2. Mueller-Muller PD based clock recovery
- 3. Minimum Mean-Squared Error (MMSE) timing recovery [This work]



 Integrating Front-End Based PD [Emami-Neyestanak, A.; Palermo, S.; Hae-Chang Lee; Horowitz, M.;, VLSI Symposium 2004] :



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• Mueller-Muller Timing Recovery [*IEEE Trans. on Comm.*, 1976; Balan JSSC 2005]



• True only for uncorrelated random data

• MMSE PD based CDR (This work):



Sign-Sign MMSE



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- <u>Advantages of MMSE:</u>
 More robust than other baud-rate techniques since there are no constraints on the input data.
- <u>Disadvantages:</u> Requires slope and error information.



Error-Signal Free Sign-Sign MMSE



$$\begin{aligned} \tau_{k+1} &= \tau_k + \theta_{bb} \operatorname{sgn}[e_k] \operatorname{sgn}\left[\frac{dy(kT + \tau_k)}{d\tau_k}\right] \\ &\approx \tau_k + \theta_{bb} \operatorname{sgn}[y(kT + \tau_k)] \operatorname{sgn}\left[\frac{dy(kT + \tau_k)}{d\tau_k}\right] \qquad \tau_{k+1} \approx \tau_k + \theta_{bb} \operatorname{sgn}\left[y(kT + \tau_k)\frac{dy(kT + \tau_k)}{d\tau_k}\right] \end{aligned}$$

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Error-Signal Free Sign-Sign MMSE

$$\tau_{k+1} = \tau_k + \theta_{bb} \operatorname{sgn}[e_k] \operatorname{sgn}\left[\frac{dy(kT + \tau_k)}{d\tau_k}\right]$$
$$\approx \tau_k + \theta_{bb} \operatorname{sgn}[y(kT + \tau_k)] \operatorname{sgn}\left[\frac{dy(kT + \tau_k)}{d\tau_k}\right]$$

$$\tau_{k+1} \approx \tau_k + \theta_{bb} \operatorname{sgn}\left[y(kT + \tau_k) \frac{dy(kT + \tau_k)}{d\tau_k} \right]$$





Slope Detection Schemes



Choice of RC time constant

• For 10-Gb/s data, the RC time constant was chosen to be 10ps: R = 200 Ω , C = 50 fF







Passive Filter



 Inductors improve bandwidth without compromising the relative phase shift between the data and slope paths.



Die Photo



0.18 µm CMOS; Die area=1.1 mm²



Measurement Results



Network Analyzer Measurements: Data Path Bandwidth (Measured)=6-GHz. S₂₁ in Slope Path increases @ 20dB/dec.



Measurement Results





Measurement Results







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Conclusions

- A passive filter that provides simultaneous low-pass and high-pass characteristics was presented.
- The high-pass transfer characteristic is utilized to provide slope information that is aligned with the low-pass data output.
- Data and slope signals from the passive filter can be used to recover a clock based on modified MMSE timing recovery.
- Prototype passive filter was used with external components to recover a 2-GHz clock from a 2-Gb/s 2³¹-1 random data sequence.



Thank you



Passive Filter



