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Pre-FEC and Post-FEC BER as Criteria for Optimizing Wireline Transceivers

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Outline

1.Motivation

2.Wireline Transceiver Model

**3.Impact of Varying FFE and DFE Tap Weights on
Pre-FEC and Post-FEC BER**

4.1/(1+D) Pre-Coding

5.Conclusion

Motivation

➤ Common receiver DSP equalizer blocks in 100Gb/s+ wireline applications:

➤ Feed-forward Equalizer (FFE)

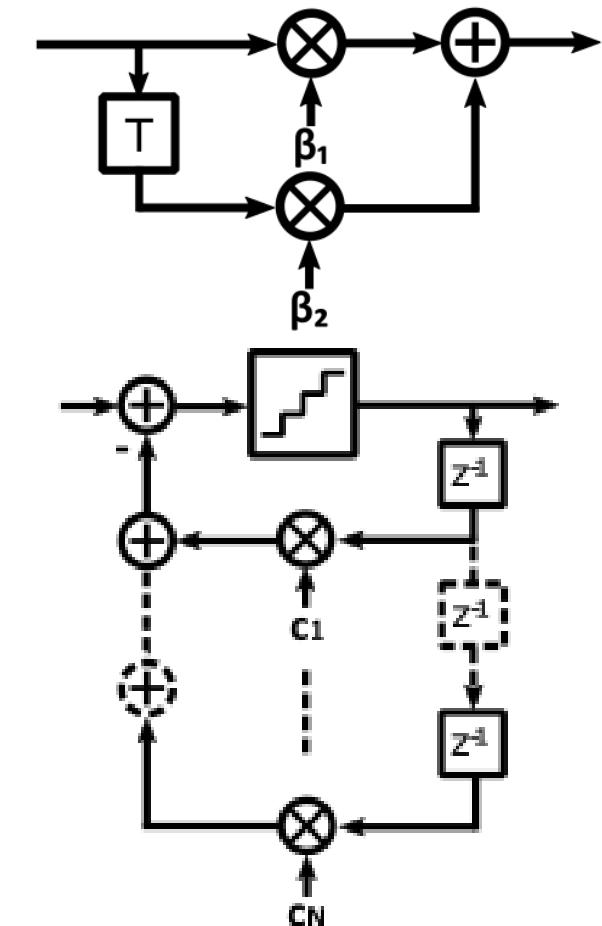
- 🔴 Noise amplification
- 🟢 High speed operation
- 🟢 No error propagation

➤ Decision-Feedback Equalizer (DFE)

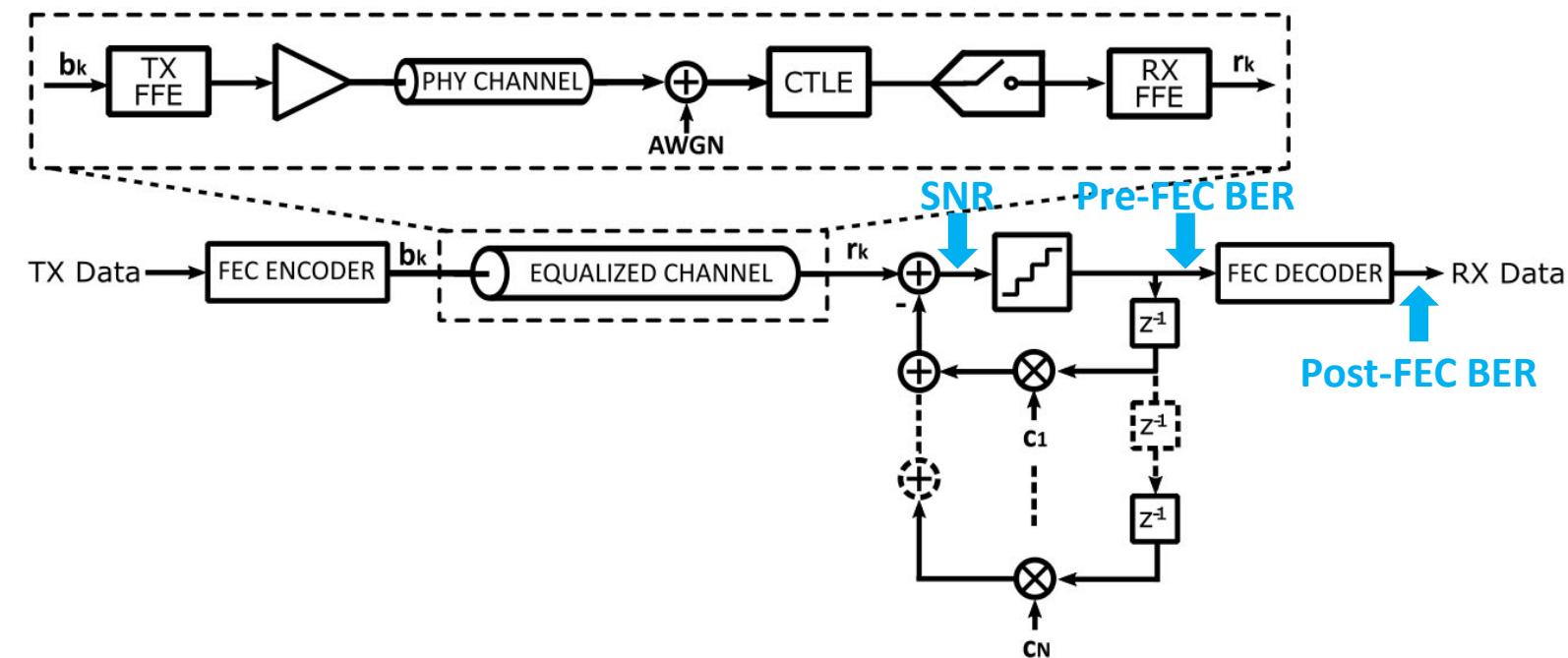
- 🔴 Error propagation
- 🔴 Speed limited by critical feedback path
- 🟢 No noise amplification

➤ Forward-Error Correction (FEC) code have also become an integral part of the DSP

- Standard Reed-Solomon (RS) to mitigate DFE error propagation
- Ex: RS(544,514,15) KP4 code to achieve a targeted post-FEC BER $<10^{-15}$



Motivation



- Three performance metrics for optimizing equalizer coefficients in wireline transceivers:
 - SNR (Implicitly the optimization criteria when using LMS adaptation)
 - Pre-FEC BER
 - Post-FEC BER

Metric	FFE Noise Amplification	DFE Error Propagation	Sensitivity to Long Burst Errors at very low BER
SNR	✓	✗	✗
Pre-FEC BER	✓	✓	✗
Post-FEC BER	✓	✓	✓

Motivation

- FFE and DFE tap coefficients are typically optimized to maximize signal-to-noise ratio (SNR) or to minimize the mean-squared error (MMSE) or pre-FEC BER [1-3]
- Equalizer parameters found by conventional methods do not necessarily minimize post-FEC BER
- This paper presents an accurate and efficient methodology for finding the impact of wireline transceiver parameters, such as equalizer coefficients, on post-FEC BER

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2. Wireline Transceiver Model

a. System Overview

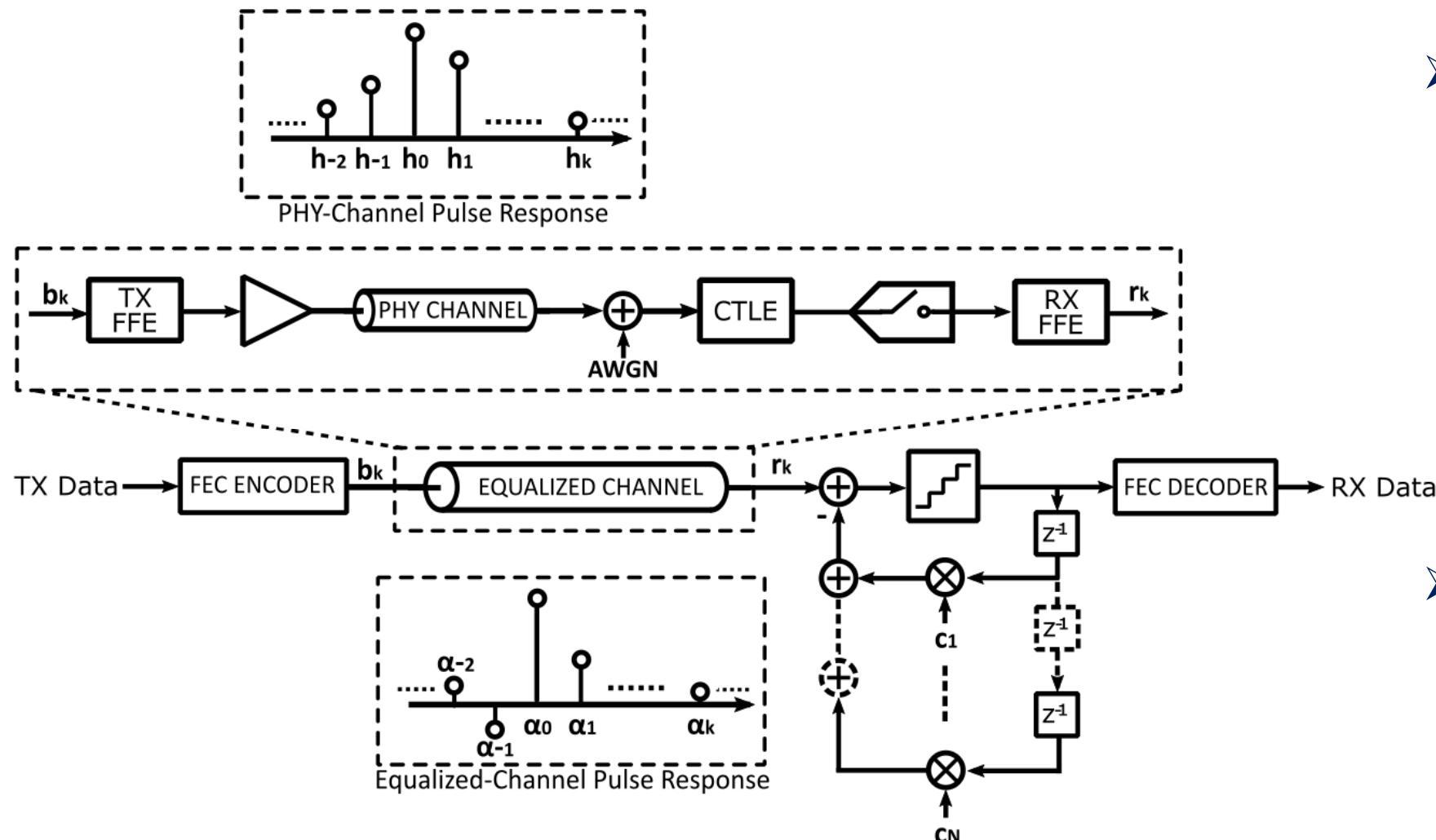
b. DFE Error Propagation

**3. Impact of Varying FFE and DFE Tap Weights on
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4.1/(1+D) Pre-Coding

5. Conclusion

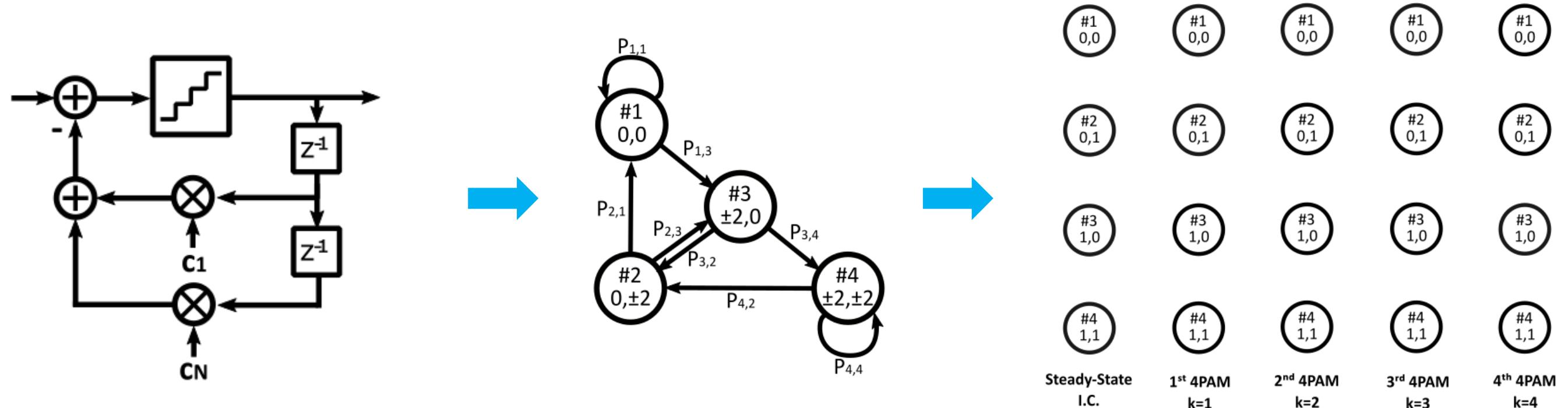
Transceiver Model – System Overview



➤ Equalized pulse response $\alpha(z)$ is generated by convolving the physical channel's pulse with the impulse response of other components in the link, such as the TX FFE, TX driver, CTLE and RX FFE

➤ Additive white Gaussian noise (AWGN) assumed at CTLE input, creating correlated noise samples after CTLE filtering

Transceiver Model – DFE Error Propagation [Yang, TCAS-I, 2020]



- Example of a 2-tap DFE represented by a simplified 4-state Markov model
- Time-unrolling the Markov DFE model to generate PAM trellis
- Apply trellis dynamic programming to the PAM trellis to efficiently collect all error patterns

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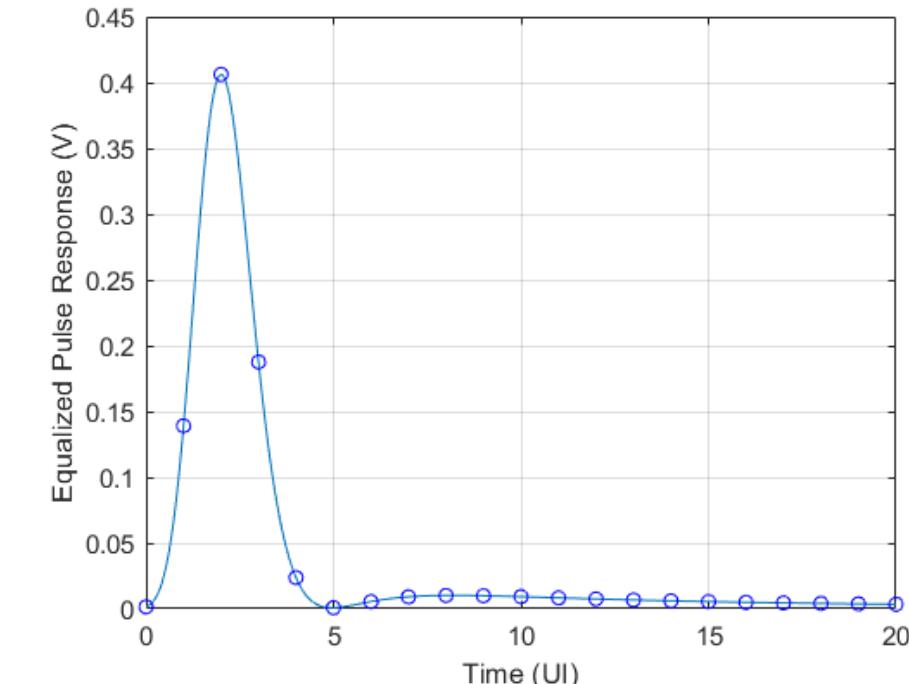
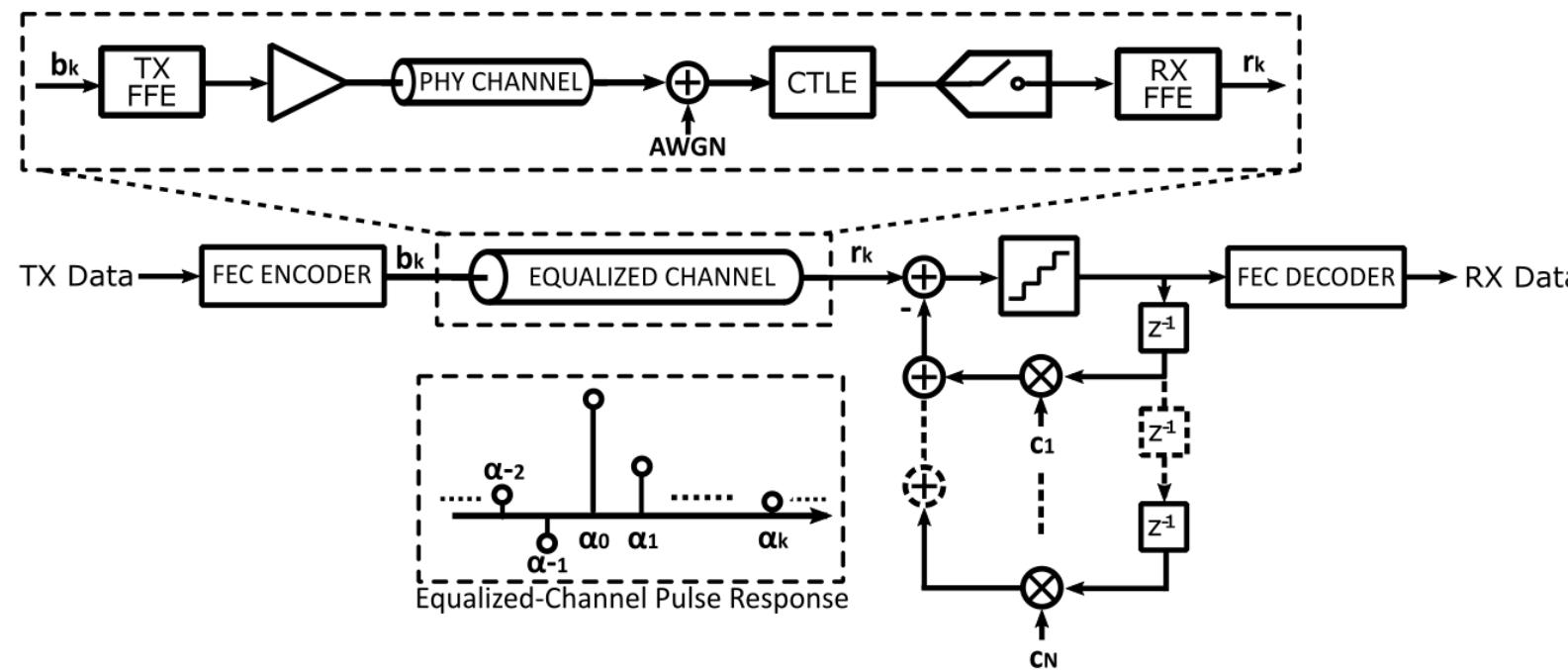
a. Pre-FEC vs Post-FEC BER Optimum

b. Simulation Results

4. 1/(1+D) Pre-Coding

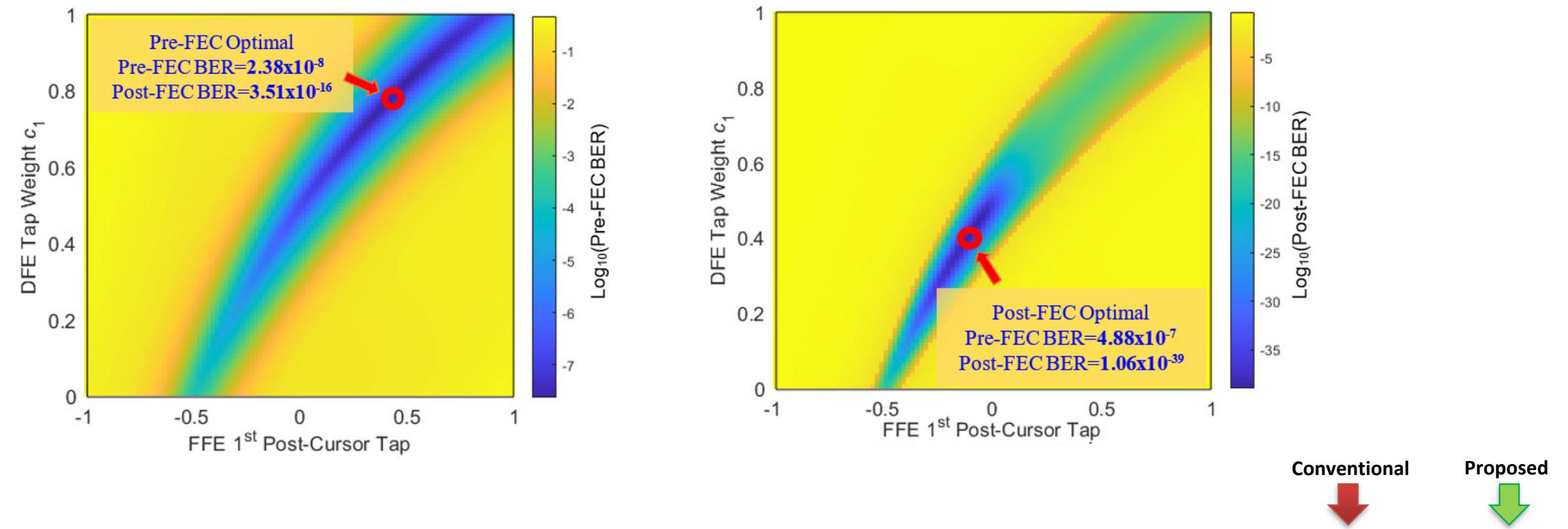
5. Conclusion

Pre-FEC vs Post-FEC BER Optimum - Link Setup



- A channel model with 30 dB insertion loss for a link communicating 4-PAM symbols at 56 GBAud/s subject to 0.55 V_{P-P} swing at TX, 4.58 mV_{rms} integrated rms noise
- A simplified CTLE model provides 12 dB peaking gain with 0 dB gain at DC
- A 1-tap DFE and a 7-tap FFE with 2 pre-cursor and 4 post-cursor taps at RX
- The post-FEC BER is calculated assuming the standard KP4 RS(544,514, 15) code

Pre-FEC vs Post-FEC BER Optimum



- Vastly different optimal point with proposed optimization approach
- Tradeoff between FFE noise amplification and DFE error propagation

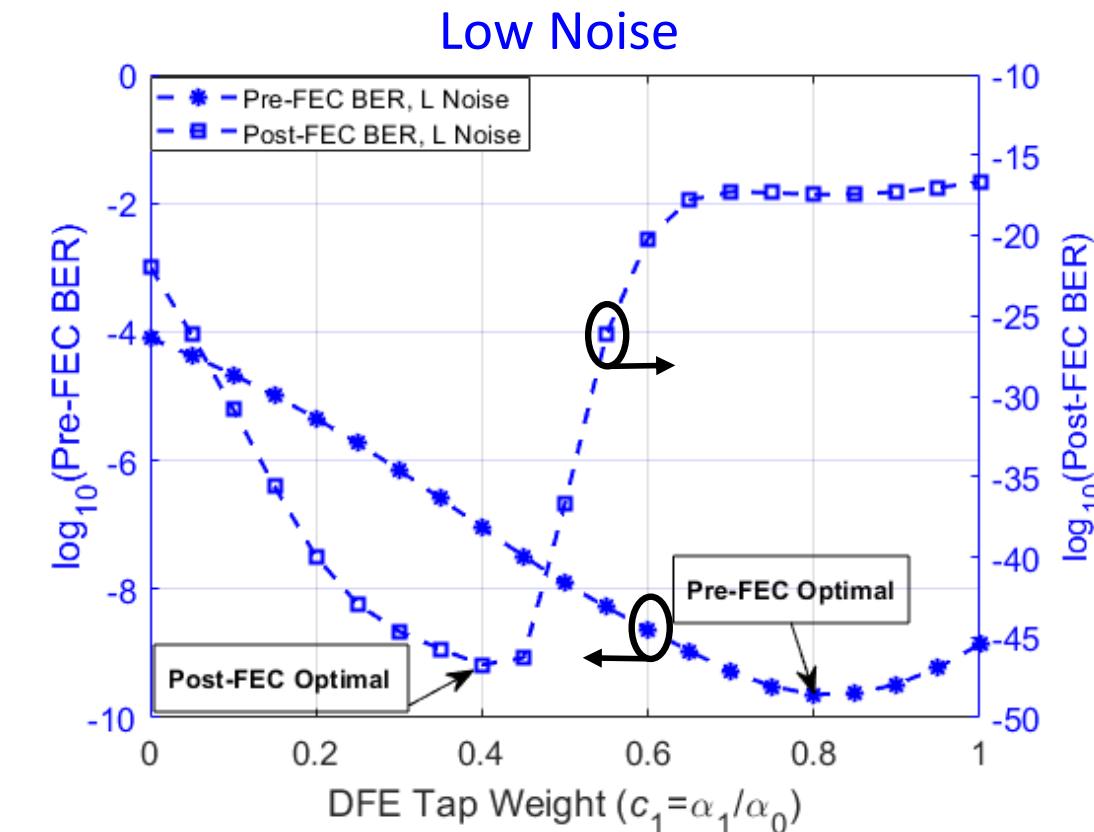
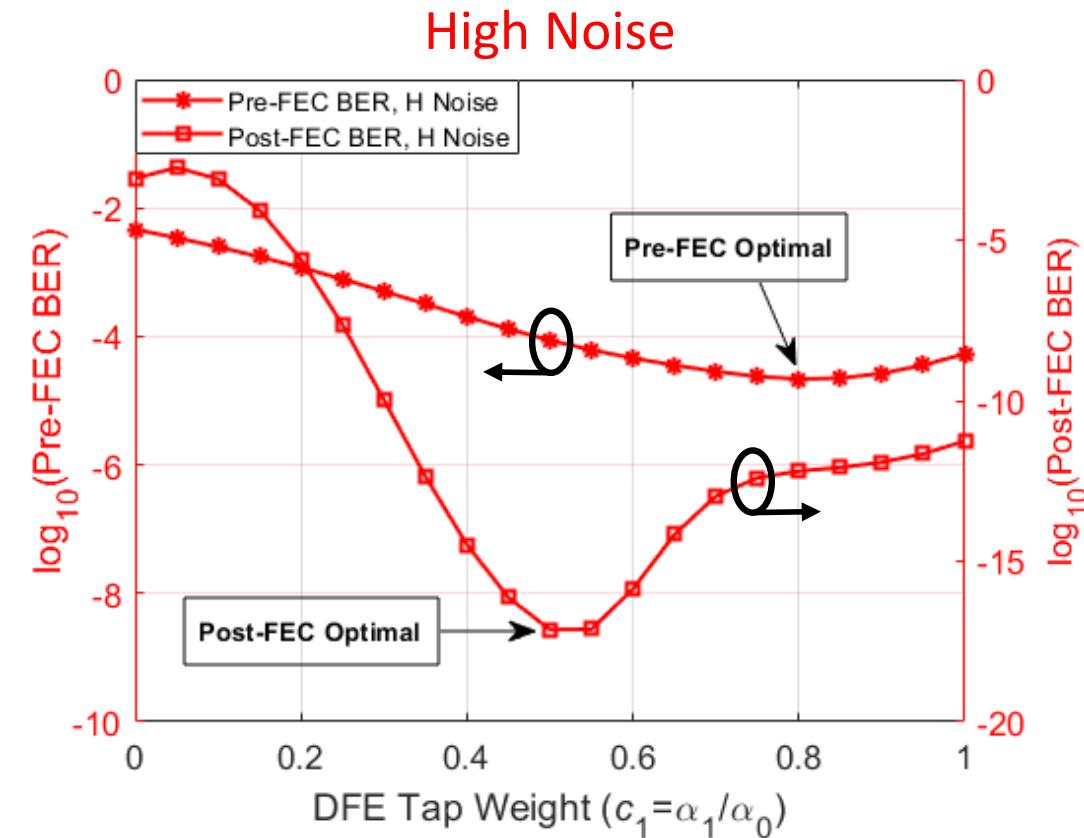
	Pre-FEC Optimization	Post-FEC Optimization
Pre-FEC BER	2.38e-8	4.88e-7
Post-FEC BER	3.51e-16	1.06e-39

Significant improvement in post-FEC BER using proposed optimization approach

Simulation Results

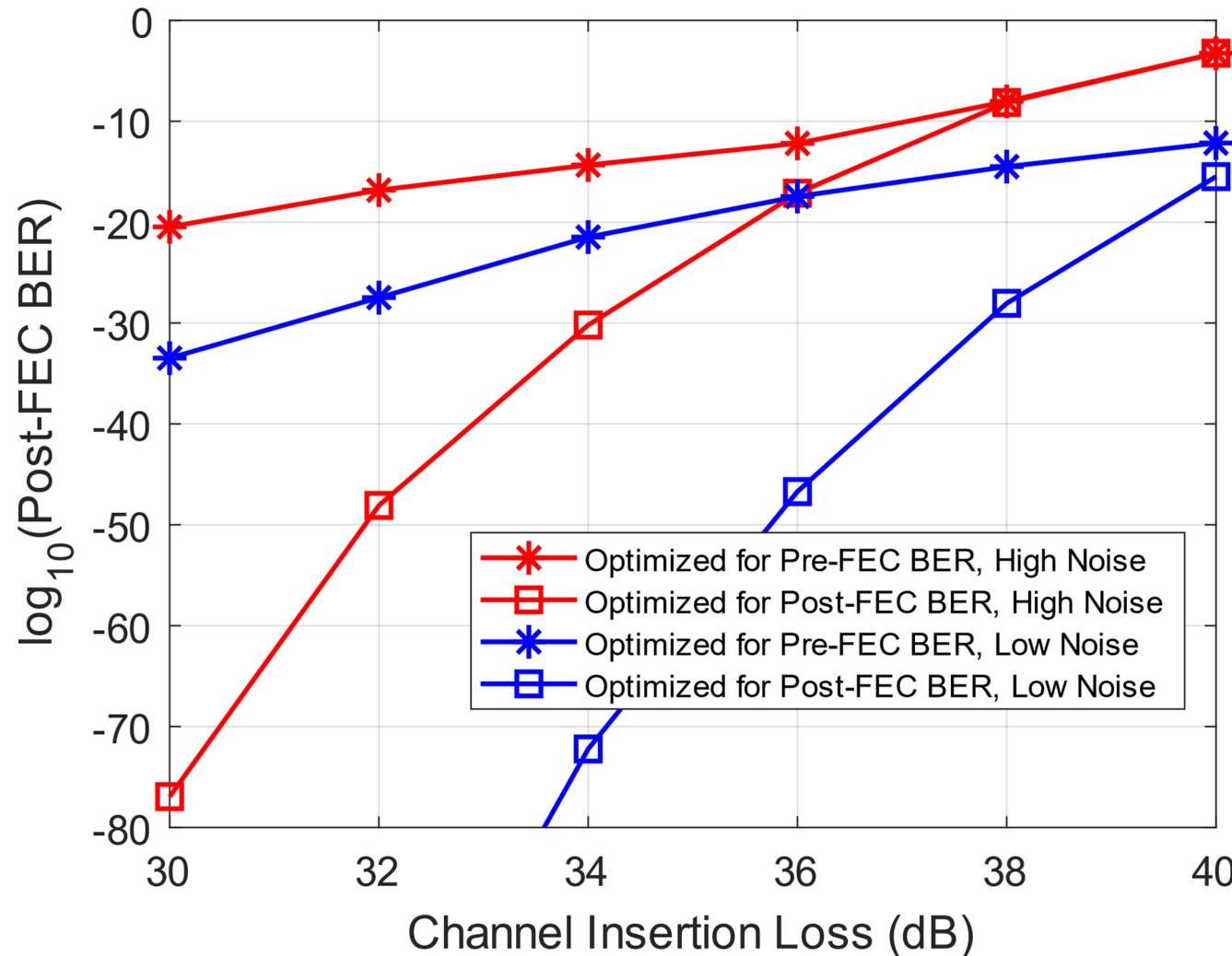
- More extensive simulation results using six measured channel responses to validate our methodology using post-FEC BER
- TX has a 2-tap FFE providing 5 dB pre-emphasis, and the RX FFE has 15 taps, including 3 pre-cursor taps and 11 post-cursor taps
- An 8th-order CTLE model was applied to equalize all six channels having 30–40 dB insertion loss
- The equalized pulse responses including TX FFE, CTLE and PHY channel are tabulated in Table I of the paper

Simulation Results



- Plot both the pre-FEC BER and post-FEC BER as a function of DFE tap weight α_1/α_0 for the 36 dB channel
- Simulated at two integrated rms noise levels: 1.62 mV_{rms} (low noise) and 2.42 mV_{rms} (high noise)
- Different DFE coefficients at pre-FEC and post-FEC optimal
 - Post-FEC BER is minimized at a lower α_1/α_0 than pre-FEC

Simulation Results



- Repeating the same analysis for all six measured channels
- The optimal post-FEC BER obtained by post-FEC optimization is always superior

Outline

1.Motivation

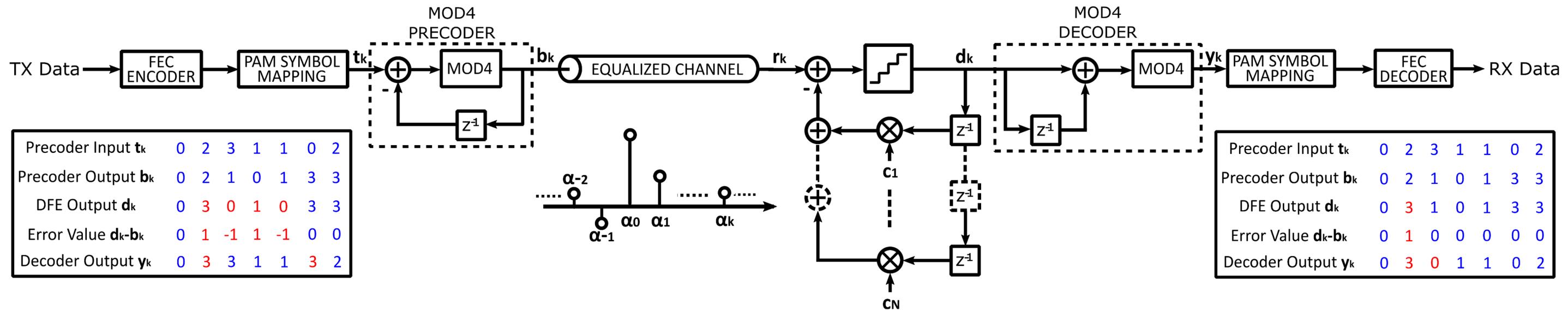
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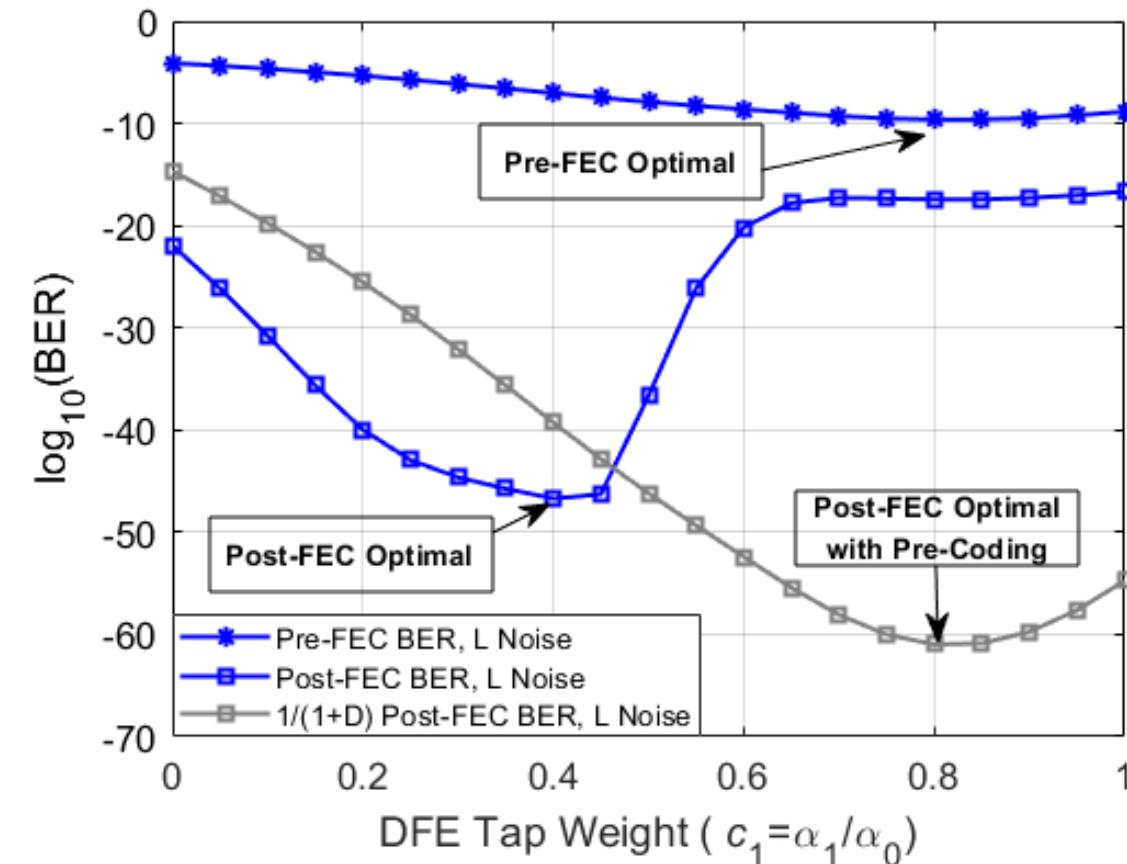
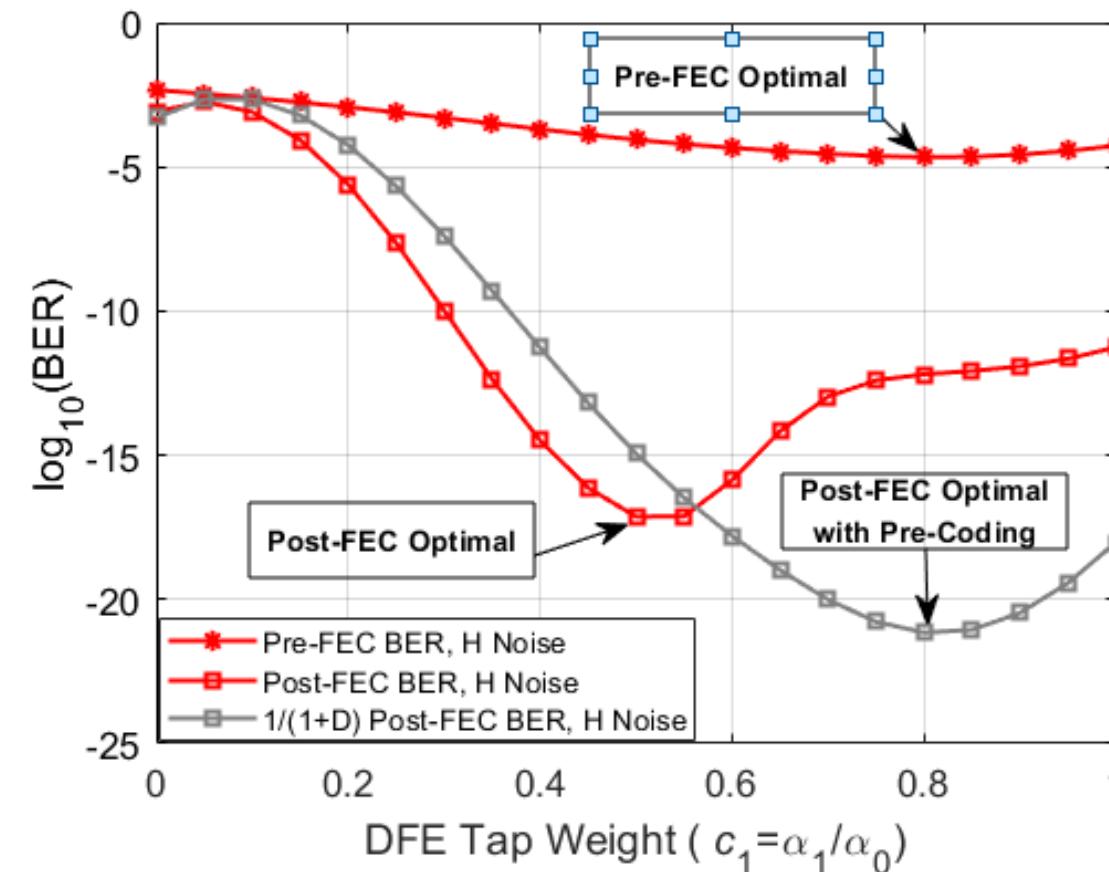
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1/(1+D) Pre-Coding



- A wireline transceiver model incorporating 1/(1+D) pre-coding to mitigate DFE error bursts
- 1/(1+D) decoder removes burst errors because the error $d_k - b_k$ in the current received symbol is added to the error $d_{k-1} - b_{k-1}$ in the previously received symbol
- Isolated individual symbol errors give rise to two consecutive symbol errors after decoding
- Method in [5] is used to generate the post-FEC BER results including 1/(1+D) pre-coding

1/(1+D) Pre-Coding



- Post-FEC BER of the previous 36dB channel case with and without 1/(1+D) pre-coding
- With pre-coding, both post-FEC and pre-FEC BER are minimized with the same equalizer coefficients

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- 5.Conclusion**

Conclusion

- Using SNR or pre-FEC BER as performance metrics may not be effective in minimizing post-FEC BER when architecting and optimizing wireline links.
- Error propagation is not accurately accounted for when SNR or pre-FEC BER are used.
- In general, links attain their minimum post-FEC BER with equalizer coefficients very different from those that minimize pre-FEC BER.
- The introduction of $1/(1+D)$ pre-coding mitigates the impact of error bursts, ensuring that both pre-FEC and post-FEC BER are minimized with the same equalizer coefficients.

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