

Chapter 9 - Problems

9.1) Show that $X(n-k) \xleftrightarrow{z} z^{-k} X(z)$

The z -transform for $x(n)$ is

$$X(z) \triangleq \sum_{n=-\infty}^{\infty} x(n) z^{-n} \quad \text{for } z \triangleq e^{sT}$$

$$= \dots + x(-1) z^{-1} + x(0) z^0 + x(1) z^1 + \dots$$

Given that $x_2(n) = x(n-k)$,

$$X_2(z) = \sum_{n=-\infty}^{\infty} x_2(n) z^{-n} = \sum_{n=-\infty}^{\infty} x(n-k) z^{-n} \quad \text{II}$$

Let $i = n-k$

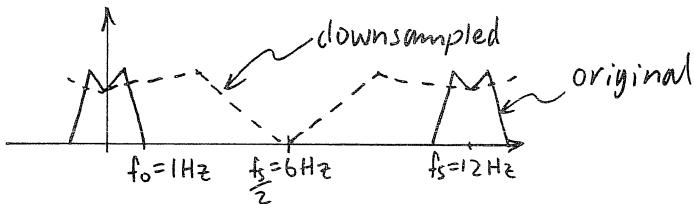
$\therefore n = i+k$ and we can rewrite II as

$$X_2(z) = \sum_{i=-\infty}^{\infty} x(i) z^{-(i+k)} = z^{-k} \underbrace{\sum_{i=-\infty}^{\infty} x(i) z^{-i}}_{= X(z)}$$

$$\therefore \underline{x_2(z) = z^{-k} X(z)}$$

Q.E.D.

9.2)



\therefore bandwidth is 1 Hz, a min. sampling rate of 2 Hz is required.

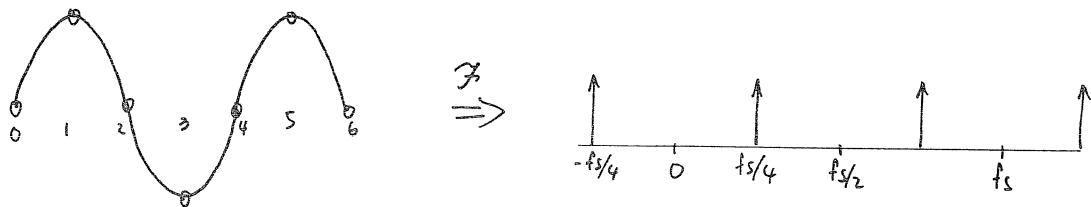
\therefore The signal can be downsampled by a factor of

$$\frac{f_s}{f_{\min}} = \frac{12 \text{ Hz}}{2 \text{ Hz}} = 6$$

9.3) Downsampling is not time-invariant.

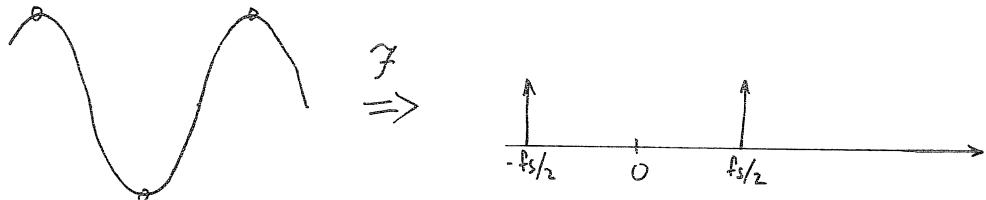
Counterexample:

Given the sampled sinusoid and its spectrum:



Consider the case where we downsample by two, done simply by discarding every other sample.

If we discard all the even samples we get, as expected,



However, by discarding all the odd samples, we are left with a constant vector of zeros, and effectively no signal.

As for linearity, downsampling is linear \Leftrightarrow

$$\text{Given } w(n) = ax(n) + by(n),$$

its downsampled equivalent, $w'(n)$, is given by

$$w'(n) = a x'(n) + b y'(n)$$

where $x'(n)$ and $y'(n)$ are equivalently downsampled equivalents of $x(n)$ and $y(n)$.

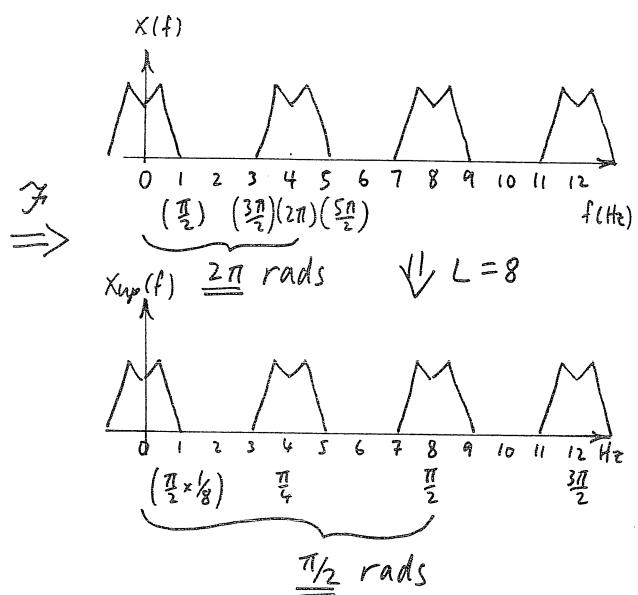
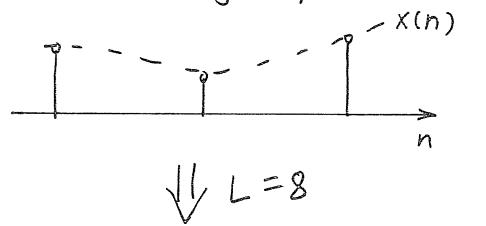
Proof: For downsampling factor of L

$$\begin{aligned} w'(n) &= w(nL+k) \quad n, L \in \mathbb{Z}, k \in [0, L-1] \\ &= \underbrace{a x(nL+k)}_{\text{But these are simply downsampled versions of}} + \underbrace{b y(nL+k)}_{x(n) \text{ and } y(n), x'(n) \text{ and } y'(n) \text{ respectively.}} \end{aligned}$$

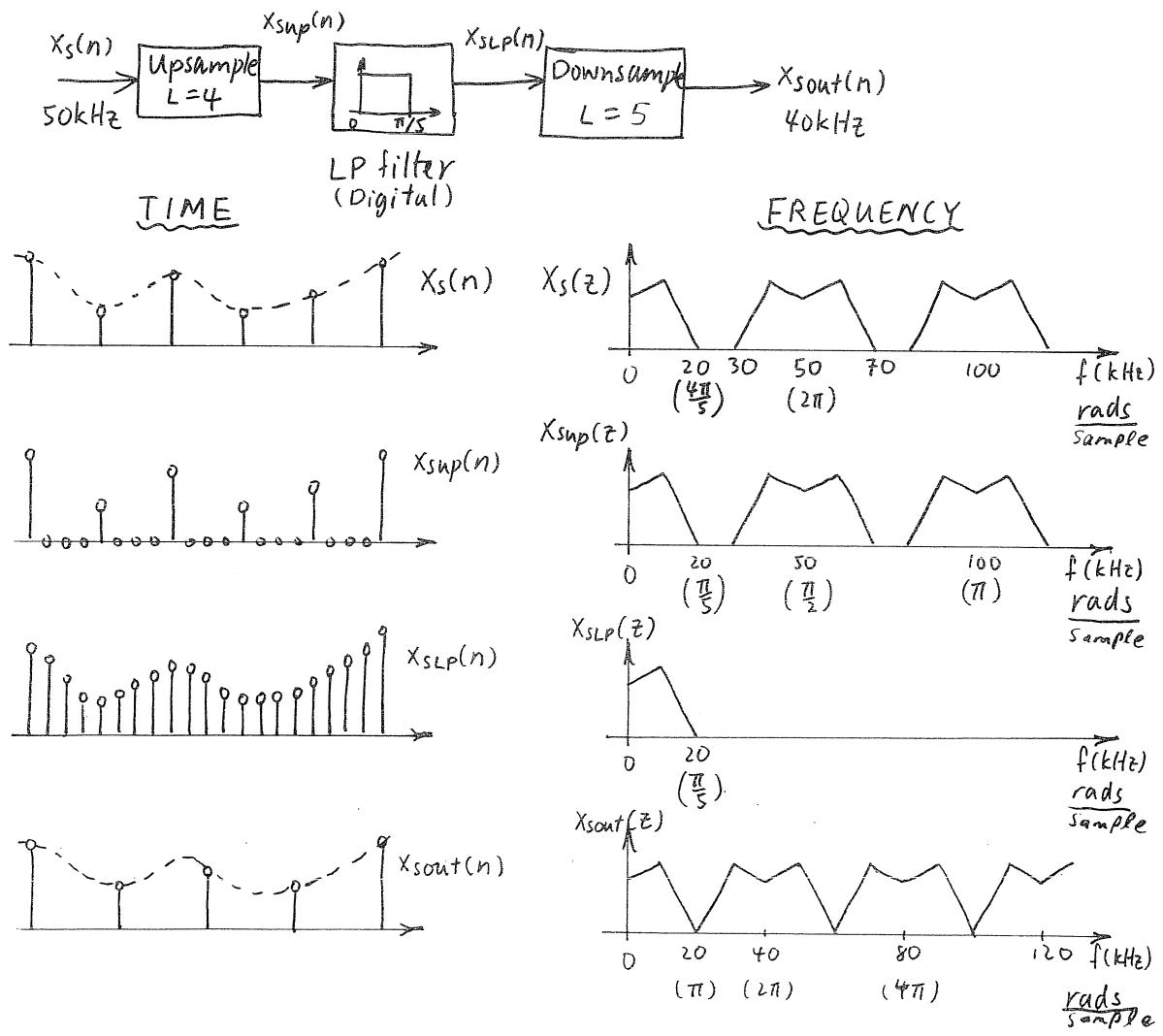
But these are simply downsampled versions of $x(n)$ and $y(n)$, $x'(n)$ and $y'(n)$ respectively.

$$\therefore w'(n) = a x'(n) + b y'(n) \quad \text{Q.E.D.}$$

9.4) Upsampling by 8 :



9.5) Block diagram of sample rate converter :



9.6) Find poles and zeros of

$$H(z) = \frac{0.05}{z^2 - 1.6z + 0.65}$$

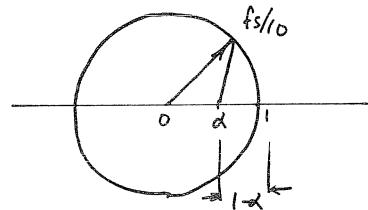
For poles : $z_p^2 - 1.6z_p + 0.65 = 0$

$$\therefore z_p = 0.8 \pm i0.1 = 0.806 \angle 7^\circ$$

By inspection, 2 zeros are at $z=0$.

9.7) Given $H(z) = \frac{K}{z-\alpha}$, $K, \alpha \in \mathbb{R}$

Find α such that $f_{-3dB} = f_s/10$.



At DC or $z=1$

$$|H(z)|_{z=1} = \frac{K}{1-\alpha} \equiv |H(\omega)|_{\omega=0} \quad \square$$

$$\text{Now } f_{-3dB} = f_s/10 \Rightarrow \omega_{-3dB} = \frac{2\pi}{10} = \pi/5 \text{ rads/sec}$$

$$\begin{aligned} \therefore |H(\omega_{-3dB})| &= |H(z)|_{z=e^{j\pi/5}} \\ &= \frac{K}{|e^{j\pi/5} - \alpha|} \quad \square \end{aligned}$$

$$\text{Now set } |H(\omega_{-3dB})| = \frac{1}{\sqrt{2}} |H(z)|_{z=1}$$

$$\therefore \frac{K}{|e^{j\pi/5} - \alpha|} = \frac{1}{\sqrt{2}} \frac{K}{|1-\alpha|}$$

$$|e^{j\pi/5} - \alpha| = \sqrt{2}(1-\alpha)$$

$$\sqrt{(\cos(\pi/5) - \alpha)^2 + \sin^2(\pi/5)} = \sqrt{2}(1-\alpha)$$

$$\cos^2(\pi/5) - 2\alpha \cos(\pi/5) + \alpha^2 + \sin^2(\pi/5) = 2\alpha^2 - 4\alpha + 2$$

$$0 = \alpha^2 + \alpha(-4 + 2\cos(\pi/5)) + 2 - 1$$

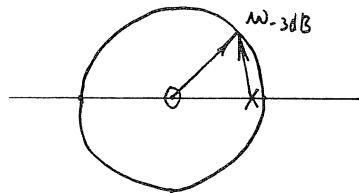
$$0 = \alpha^2 - 2.382\alpha + 1$$

$$\therefore \alpha = \underbrace{1.837}_{\text{unstable root}}$$

$$\text{or } \boxed{0.544}$$

\therefore the pole is located
at $z = 0.544$

9.8) Sketch $|H(z)|$ given $H(z) = \frac{0.05z}{z - 0.95}$



\therefore the zero is located at $z=0$,
it does not affect the
magnitude response

$$|H(z)| \Big|_{z=e^{j0}} = \frac{0.05}{0.05} = \underline{0 \text{ dB}}$$

$$|H(z)| \Big|_{z=e^{j\pi}} = \frac{-0.05}{-1.05} = \underline{-26.4 \text{ dB}}$$

For ω_{-3dB} ,

$$|H(\omega_{-3dB})| = \frac{1}{\sqrt{2}} |H(z)| \Big|_{z=e^{j0}}$$

$$\frac{0.05}{|e^{j\omega_{-3dB}} - 0.95|} = \frac{1}{\sqrt{2}}$$

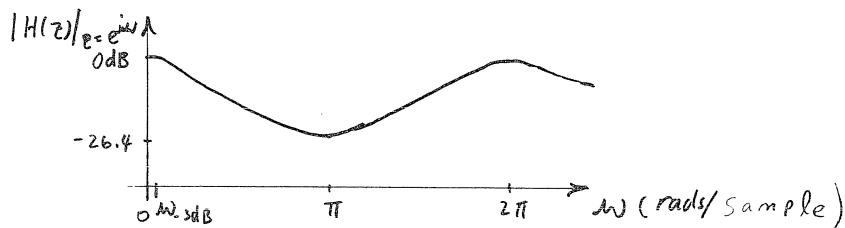
$$(\sqrt{2} \times 0.05)^2 = (\cos(\omega_{-3dB}) - 0.95)^2 + \sin^2(\omega_{-3dB})$$

$$0.005 = 1 - 1.9 \cos(\omega_{-3dB}) + 0.95^2$$

$$\cos \omega_{-3dB} = 0.99868$$

$$\therefore \underline{\omega_{-3dB} = 0.051 \text{ rads/sample}}$$

And the frequency response is



9.9) Given $y(n) = u(n) - 0.3y(n-1)$, determine the impulse response.

$$\text{Now } u(n) = \begin{cases} 1 & n=1 \\ 0 & \text{otherwise} \end{cases}$$

$$y(0) = 0$$

$$y(1) = u(1) = 1$$

$$y(2) = -0.3y(1) = -0.3$$

$$y(3) = -0.3y(2) = (-0.3)^2$$

⋮

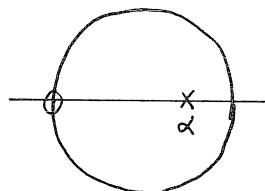
$$\therefore y(n) = \begin{cases} 0 & n=0 \\ (-0.3)^{n-1} & n>0 \end{cases} \quad \text{Impulse response}$$

9.10) Find $H(z)$.

DC gain = 1

From the basic information,
we know that

$$H(z) = k \times \frac{z+1}{z-\alpha}$$



$$\text{For } k, |H(z)||_{z=1} = k \frac{2}{1-\alpha} \equiv 1$$

$$\therefore k = \frac{1-\alpha}{2}$$

$$\text{For } \alpha, |H(z)||_{z=e^{j\omega_3dB}} = \frac{1}{\sqrt{2}} |H(z)||_{z=e^{j0}} \quad \text{where } \omega_3dB = 2\pi/30 = \pi/15$$

$$\frac{1-\alpha}{2} \times \frac{|e^{j\pi/15} + 1|}{|e^{j\pi/15} - \alpha|} = \frac{1}{\sqrt{2}}$$

$$\frac{2}{(1-\alpha)^2} = \frac{(\cos \pi/15 + 1)^2 + \sin^2 \pi/15}{(\cos \pi/15 - \alpha)^2 + \sin^2 \pi/15} = \frac{3.9563}{\alpha^2 - 1.9563\alpha + 1}$$

$$0 = (3.9563 - 2)\alpha^2 + 2 \times (1.9563 - 3.9563)\alpha + (3.9563 - 2)$$

$$0 = \alpha^2 - 2.0447\alpha + 1$$

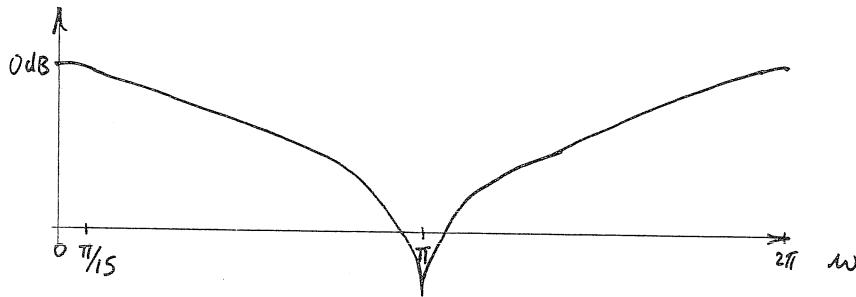
$$\therefore \alpha = 0.8098$$

$$\text{and } k = \frac{1-0.8098}{2} = 0.095$$

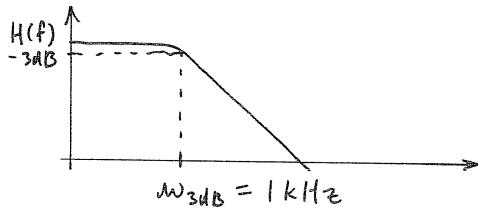
(cont.)

9.10) (cont.)

$$\therefore H(z) = \frac{0.095(z+1)}{z - 0.8098}$$



9.11)



$$f_s = 100 \text{ kHz}$$

$$Q = 1/\sqrt{2}$$

$\omega_{3dB} = 1 \text{ kHz}$ corresponds to $\frac{2\pi}{100} = \pi/50 \text{ rads/sample}$ in the z-plane

The design is done in the p-plane where ω_{3dB} is mapped to

$$\Omega_{3dB} = \tan(\pi/50 \times 1/2)$$

$$\Omega_{3dB} = 0.03143 \text{ rads/sec}$$

$$\begin{aligned} \therefore H_p(p) &= \frac{\Omega_{3dB}^2}{p^2 + \frac{\Omega_{3dB}}{Q} p + \Omega_{3dB}^2} = \frac{0.03143^2}{p^2 + \frac{0.03143}{1/\sqrt{2}} p + 0.03143^2} \\ &= \frac{9.88 \times 10^{-4}}{p^2 + 4.44 \times 10^{-2} p + 9.88 \times 10^{-4}} \end{aligned}$$

Convert this function to the z-plane using $p = \frac{z-1}{z+1}$

$$\begin{aligned} \therefore H(z) &= 9.88 \times 10^{-4} \left[\left(\frac{z-1}{z+1} \right)^2 + 4.44 \times 10^{-2} \left(\frac{z-1}{z+1} \right) + 9.88 \times 10^{-4} \right]^{-1} \\ &= \frac{9.88 \times 10^{-4} (z+1)^2}{(1 + 9.88 \times 10^{-4} + 4.44 \times 10^{-2}) z^2 + (2 \times 9.88 \times 10^{-4} - 2) z + (1 - 4.44 \times 10^{-2} + 9.88 \times 10^{-4})} \\ \therefore H(z) &= \frac{9.45 \times 10^{-4} (z+1)^2}{z^2 - 1.91 z + 0.915} \end{aligned}$$

q.12) Given the integrator transfer function,

$$\frac{Y(z)}{X(z)} = \frac{1}{z-1}$$

determine the output to a sinusoidal input.

$$\frac{Y(z)}{X(z)} = \frac{1}{z-1}$$

$$\therefore zY(z) - Y(z) = X(z)$$

$$\Rightarrow \underline{y(n+1) = x(n) + y(n)}$$

Assume $y(0) = 0$

$$\therefore y(1) = x(0) + y(0) = 1 + 0 = 1$$

$$y(2) = 0 + 1 = 1$$

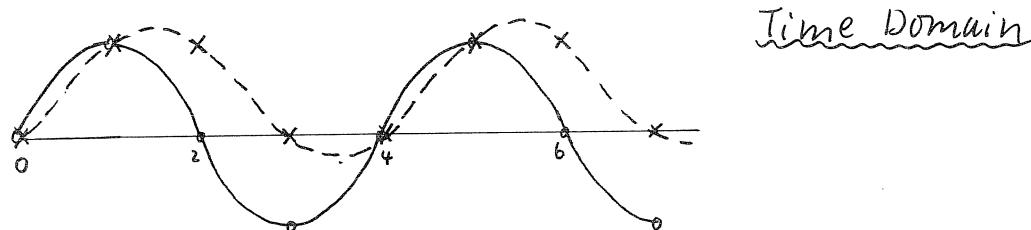
$$y(3) = -1 + 1 = 0$$

$$y(4) = 0 + 0 = 0$$

$$y(5) = 1 + 0 = 1$$

$$y(6) = 0 + 1 = 1$$

$$y(7) = -1 + 1 = 0 \quad \dots$$



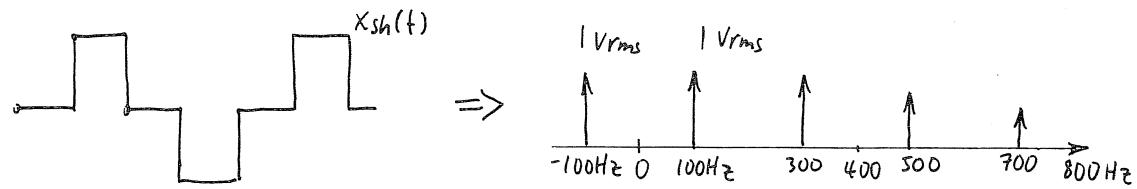
$$H(z)|_{z=e^{j\pi/2}} = \frac{1}{j+1} = \frac{1}{\sqrt{2}} e^{-j45^\circ} \quad \text{frequency domain}$$

Interpolating the output samples, we see a phase shift of 45° and the amplitude looks about 3dB lower.

Thus our time and frequency domain results are consistent.

The dc shift is due to the initial state being 0.

9.13)



$$H_{SH}(f)|_{f=100Hz} = T \left| \frac{\sin(\pi f/f_s)}{\pi f/f_s} \right|_{f=100Hz} = T \cdot \left| \frac{\sin(\frac{100\pi}{400})}{100\pi/400} \right| \\ = 0.9003 T \equiv 1 V_{rms}$$

$$H_{SH}(f)|_{f=300Hz} = T \left| \frac{\sin(3\pi/4)}{3\pi/4} \right| = 0.3001 T = 0.33 V_{rms}$$

$$H_{SH}(f)|_{f=500Hz} = T \left| \frac{\sin(5\pi/4)}{5\pi/4} \right| = 0.1801 T = 0.2 V_{rms}$$

$$H_{SH}(f)|_{f=700Hz} = T \left| \frac{\sin(7\pi/4)}{7\pi/4} \right| = 0.1286 T = 0.14 V_{rms}$$

9.14) 100Hz signal is now created with a sample rate of 10kHz.



∴ We have 100 points/period

$$H_{SH}(f) = T \left| \frac{\sin(\pi f/f_s)}{\pi f/f_s} \right|$$

$$H_{SH}(f)|_{f=100Hz} = T \times \left| \frac{\sin(\frac{100\pi}{10000})}{100\pi/10000} \right| = 0.9998 T = 1 V_{rms}$$

For the images,

$$H_{SH}(f)|_{f=9.9kHz} = T \left| \frac{\sin(\frac{9900\pi}{10000})}{9900\pi/10000} \right| = 1.01 \times 10^{-2} T = 10.1 mV_{rms}$$

$$H_{SH}(f)|_{f=10.1kHz} = T \left| \frac{\sin(\frac{10100\pi}{10000})}{10100\pi/10000} \right| = 0.99 \times 10^{-2} T = 9.9 mV_{rms}$$

9.15) Repeat Example 9.8 with $f_{in} = 100 \text{ Hz}$

For $|H(z)|$,

$$z_{in} = e^{j(2\pi \times 100/50000)} = e^{j\pi/250} = 0.99992 \pm j0.01257$$

$$\therefore |H(z_{in})| = \frac{0.2}{|(0.99992 - 0.8) + j0.01257|} = \frac{0.2}{0.20032} = \underline{0.9984}$$

This is the same for the images.

For the sample-hold circuitry,

$$H_{SH}(f)|_{f=100 \text{ Hz}} = T \frac{|\sin(100\pi/50000)|}{100\pi/50000} = 0.99999T$$

$$H_{SH}(f)|_{f=99.9 \text{ kHz}} = T \frac{|\sin(99900\pi/50000)|}{99900\pi/50000} = 1.001 \times 10^{-3}T$$

$$H_{SH}(f)|_{f=100.1 \text{ kHz}} = T \frac{|\sin(100100\pi/50000)|}{100100\pi/50000} = 9.99 \times 10^{-4}T$$

$$\therefore |y_{sh}(t)||_{f=100 \text{ Hz}} = 0.9984 \times 0.99999T \times \frac{1}{T} \times 1.0 \text{ Vrms}$$

$$= \underline{998 \text{ mVrms}}$$

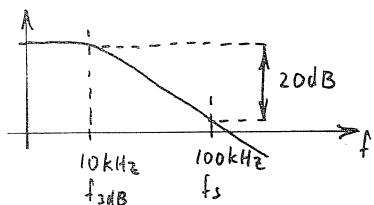
$$|y_{sh}(t)||_{f=99.9 \text{ kHz}} = 0.9984 \times 1.001 \times 10^{-3} \times 1 \text{ Vrms}$$

$$= \underline{0.999 \text{ mVrms}}$$

$$|y_{sh}(t)||_{f=100.1 \text{ kHz}} = 0.9984 \times 9.99 \times 10^{-4} \times 1 \text{ Vrms}$$

$$= \underline{0.997 \text{ mVrms}}$$

9.16)



$$|H(\omega)||_{\omega=100 \text{ kHz}} = \frac{1}{|10j+1|} = \frac{1}{10.05}$$

$$= \underline{-20.0 \text{ dB}}$$

\therefore 20 dB of attenuation is already provided by the microphone at 100 kHz.

\therefore Another 60 dB of attenuation is required from the anti-aliasing filter to obtain 80 dB noise rejection.