

A 19-GHz Broadband Amplifier Using a g_m -Boosted Cascode in 0.18- μm CMOS

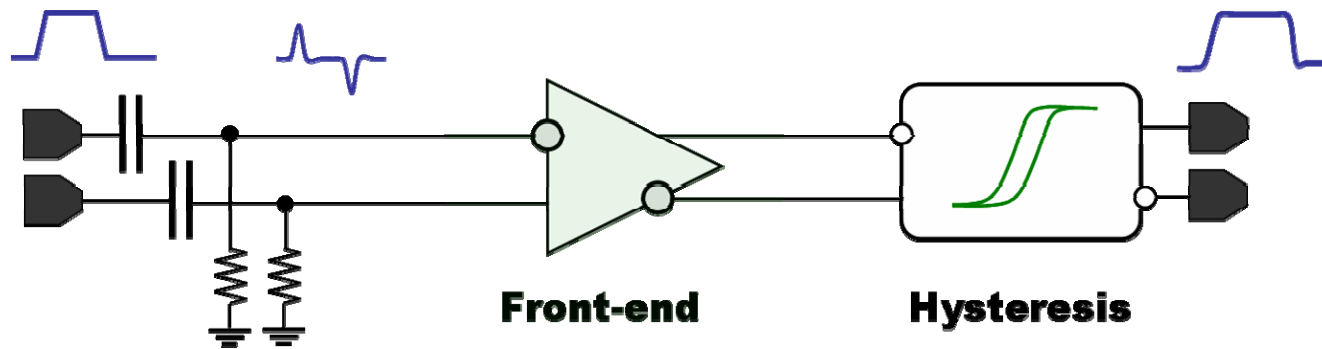
Masum Hossain & Anthony Chan Carusone
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University of Toronto

Outline

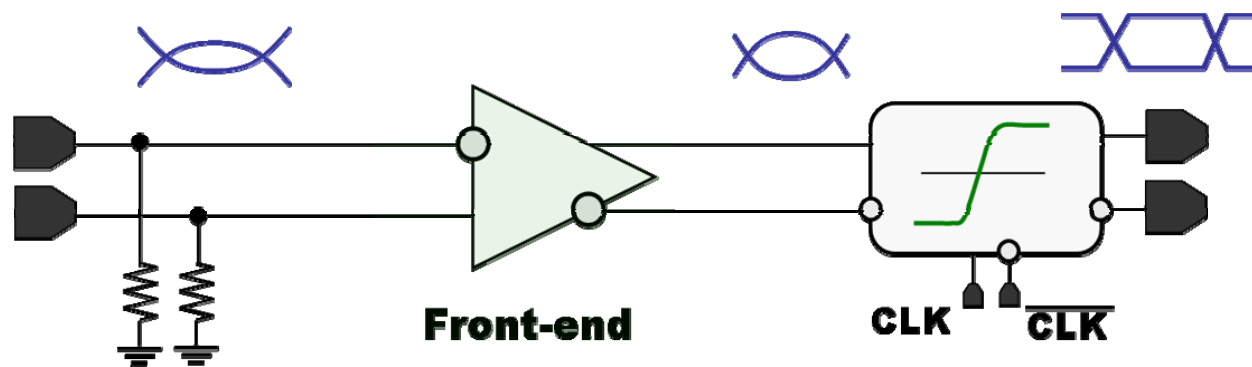
- Applications
- g_m -Boosting for bandwidth enhancement
- Differential pre-amplifier employing passive g_m -boosting
- Full front end amplifier
- Conclusions

Applications

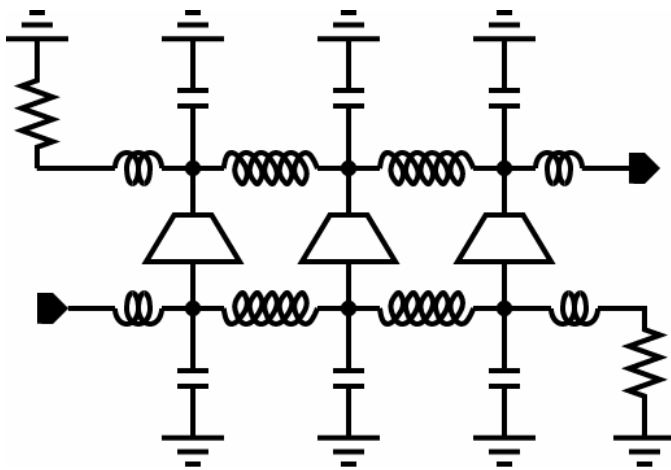
AC-coupled receiver front end:



Serial link receiver front end:

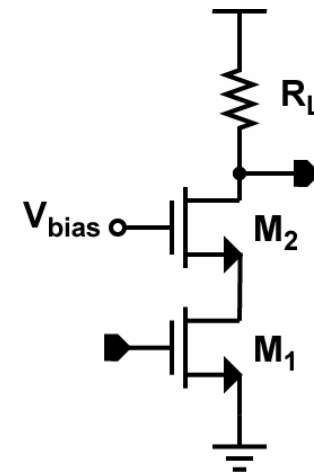


Pre-amp Topology



Distributed Amplifier

- ✓ High bandwidth
- ✗ Large area
- ✗ High power consumption
- ✗ Difficult to achieve constant group delay

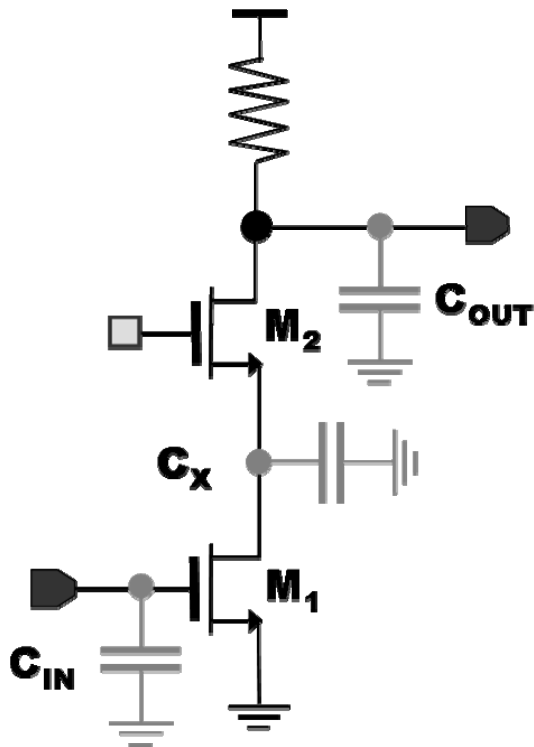


Cascode Amplifier

- ✓ Low power
- ✗ High VDD due to stacked transistors
- ✗ Bandwidth limited by node capacitances

Standard CMOS Cascode

3 time constants of simple cascode:

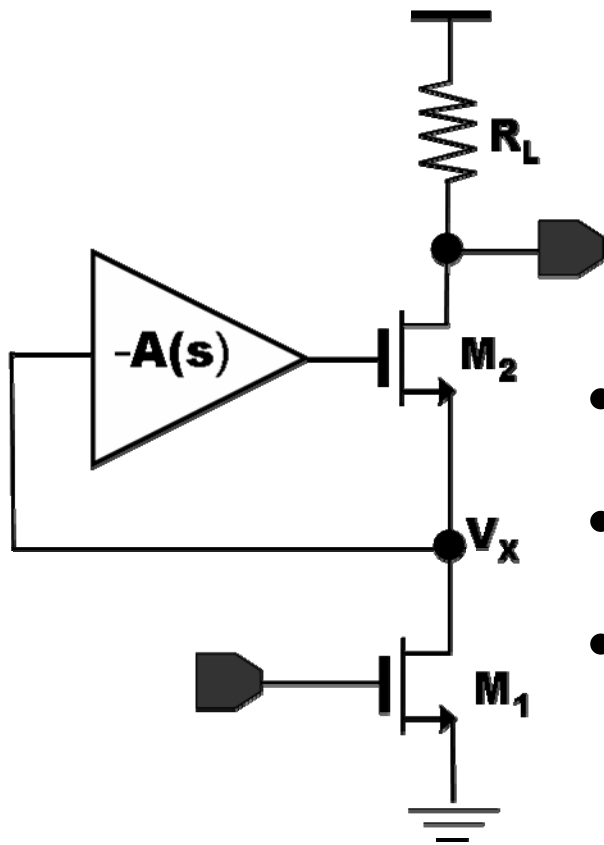


$$\tau_{\text{out}} = (R_L \parallel r_0) C_{\text{OUT}}$$

$$\tau_{\text{cascode}} = \frac{C_{\text{GS2}} + C_{\text{DB1}} + C_{\text{SB2}} + 2C_{\text{GD1}}}{g_{\text{m2}}} = \frac{C_{\text{X}}}{g_{\text{m2}}}$$

$$\tau_{\text{input}} = R_{\text{in}} C_{\text{in}}$$

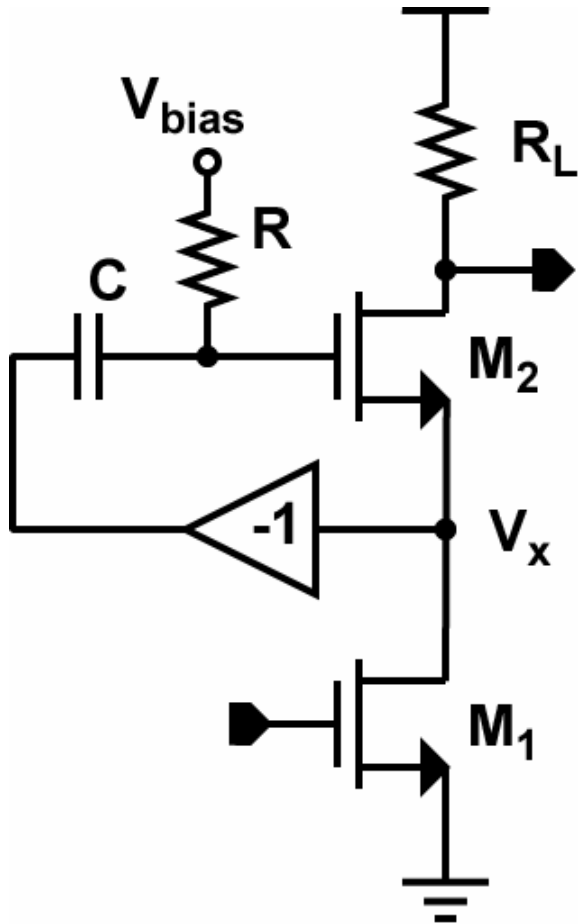
g_m -Boosted Cascode



$$g_{m_{eff}} = [1 + A(s)] g_m$$

- Increases output resistance
- **Reduces time constant at V_x**
- **Ameliorates Miller effect at the input**

g_m -Boosted Cascode



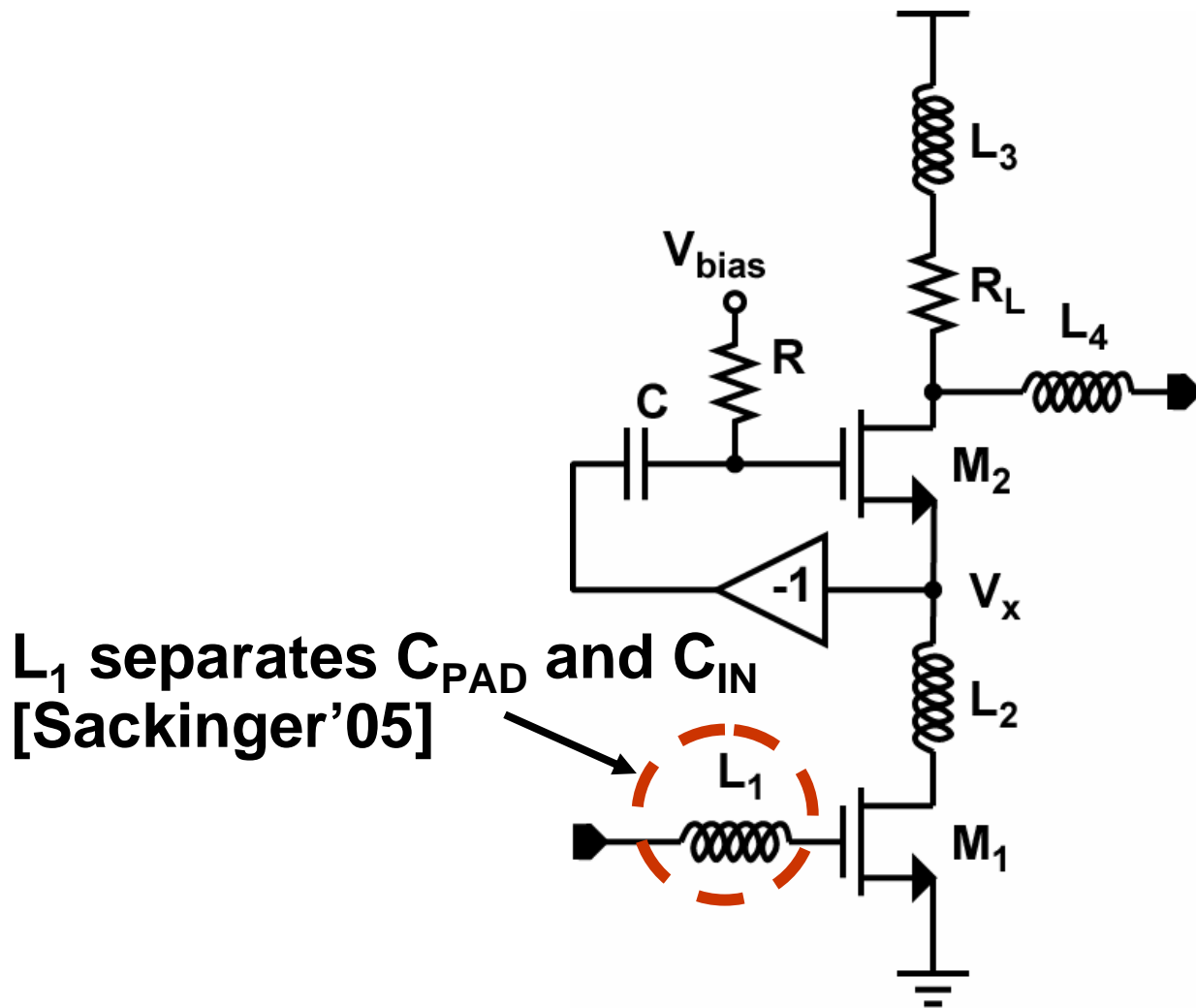
Passive g_m -boosting:

$$g_{meff} = [1 + A(s)] g_m$$

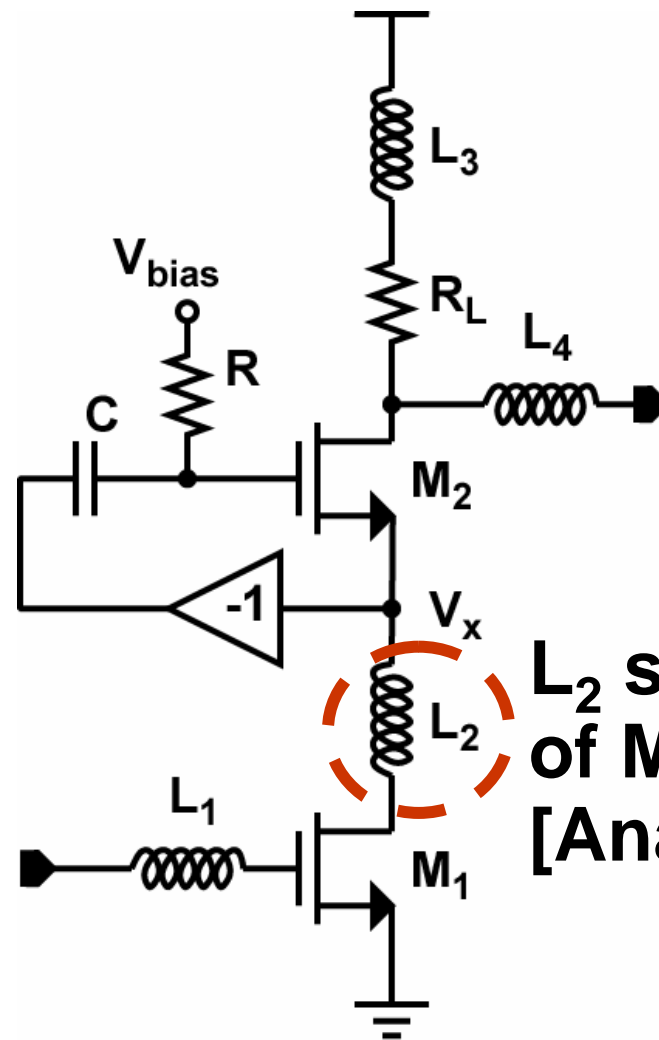
$$g_{meff} = g_m \quad \text{for } s = 0$$

$$g_{meff} = 2g_m \quad \text{for } s = \infty$$

g_m -Boosted Cascode

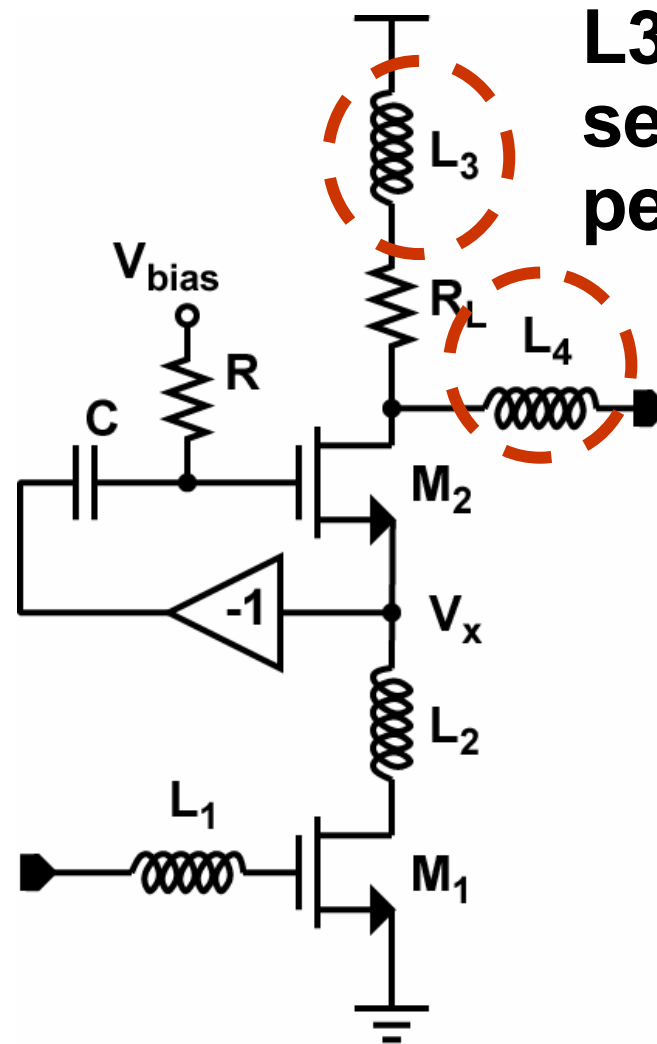


g_m -Boosted Cascode



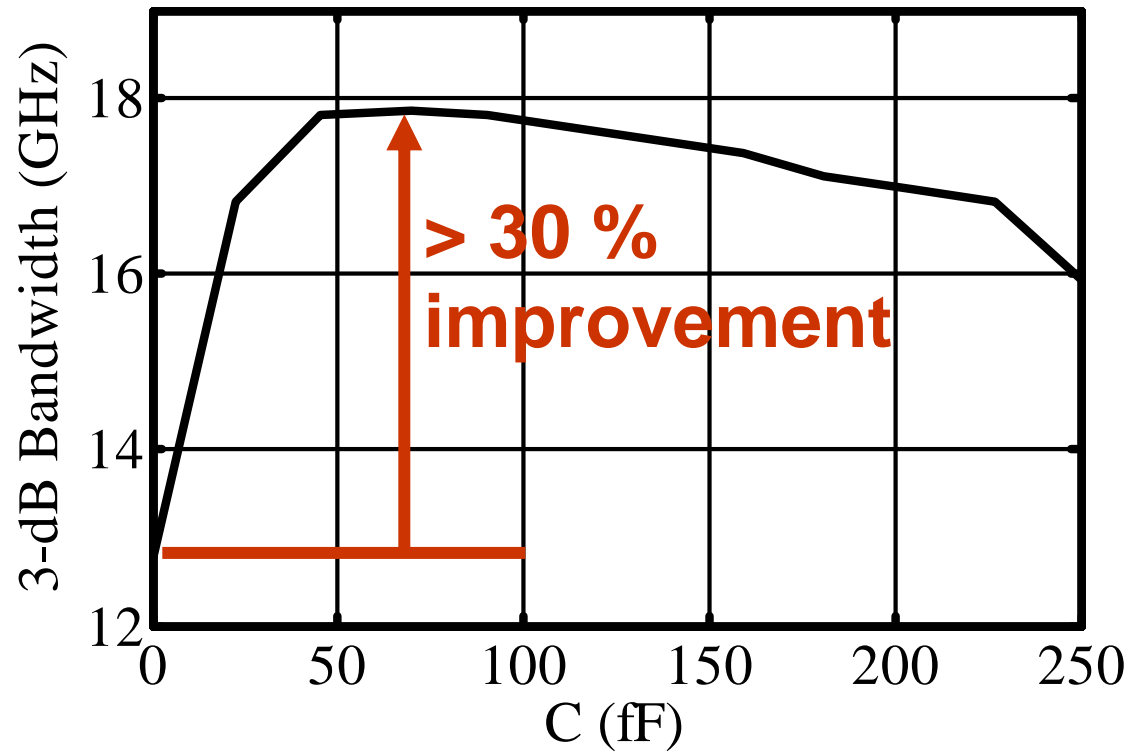
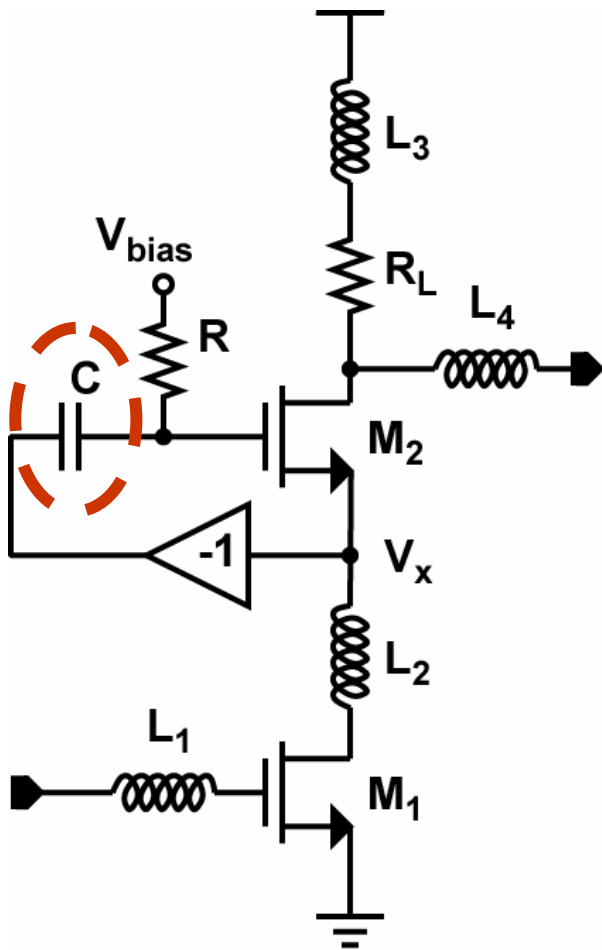
L_2 separates the C_D of M_1 and C_S of M_2 [Analui'04]

g_m -Boosted Cascode



L3 and L4 provide series and shunt peaking [Lee'04]

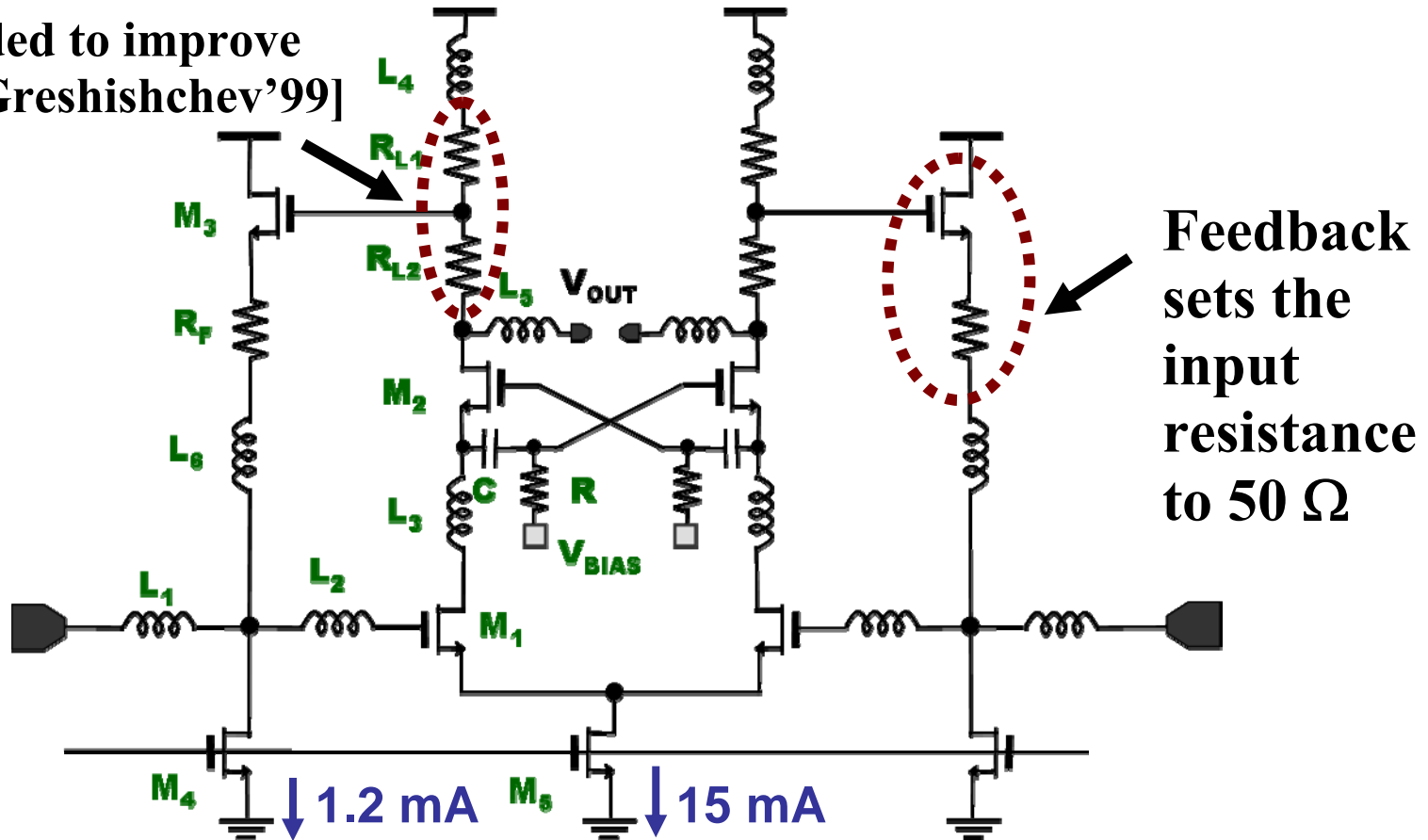
g_m -Boosted Cascode



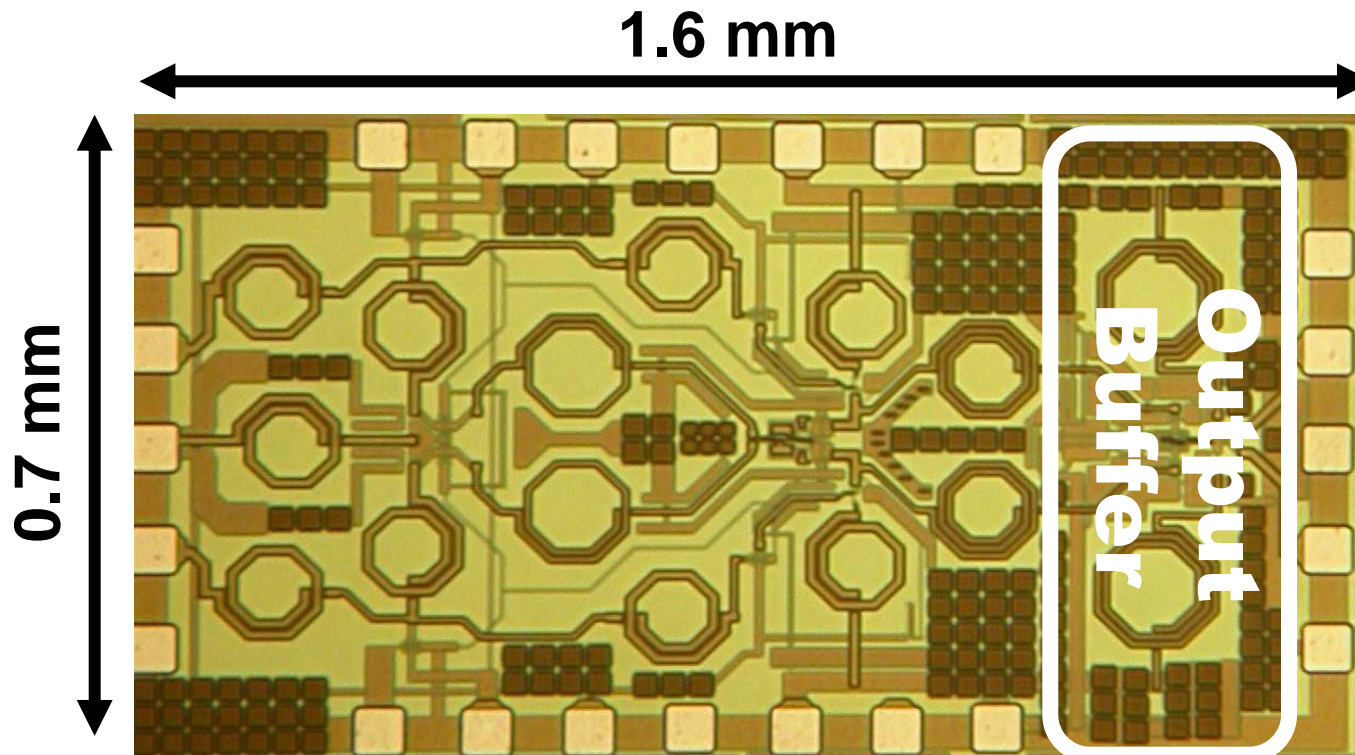
$R = 500\Omega$

Differential g_m -Boosted Cascode

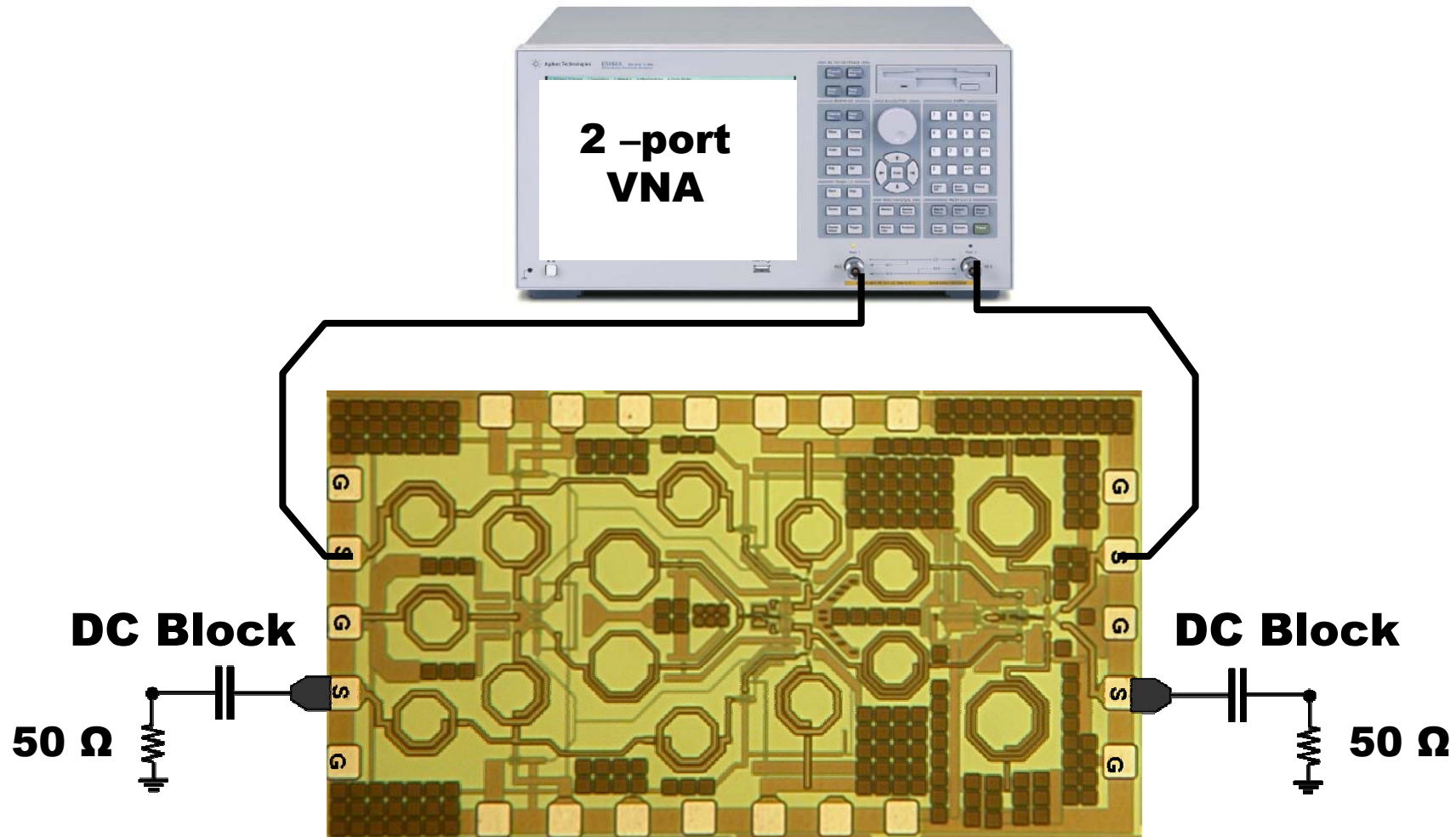
R_L is divided to improve the BW [Greshishchev'99]



Differential g_m -Boosted Cascode

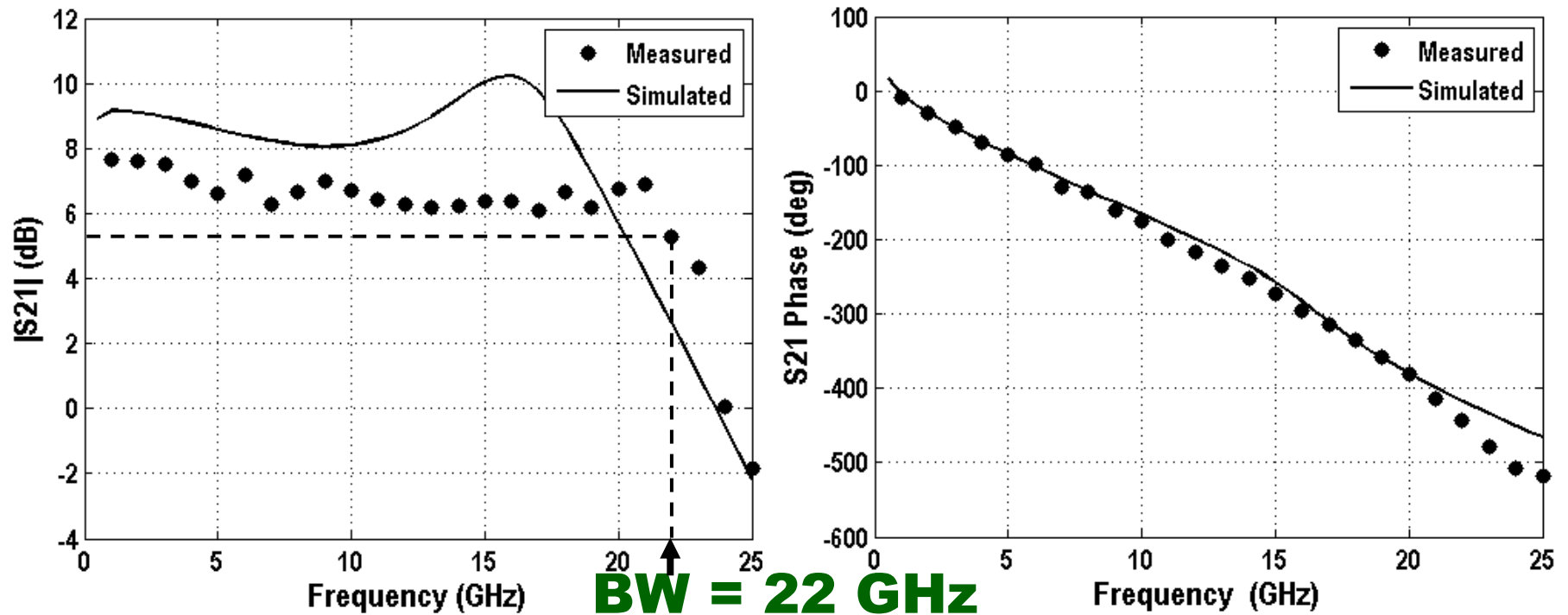


Measurement of g_m -Boosted Pre-amp



Measurement of g_m -Boosted Pre-amp

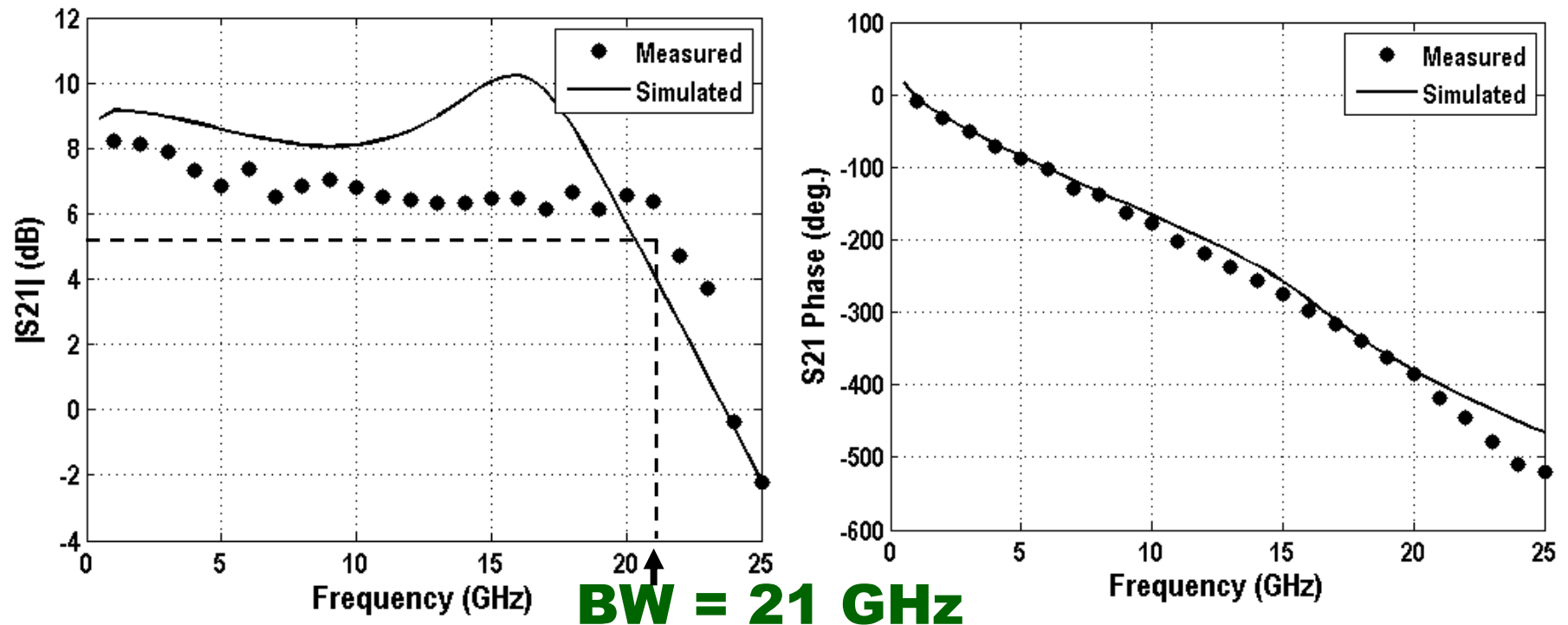
$$V_{DD} = 2.5 \text{ V}$$



6 dB was added to the S_{21} measured on a 2-port network analyzer

Measurement of g_m -Boosted Pre-amp

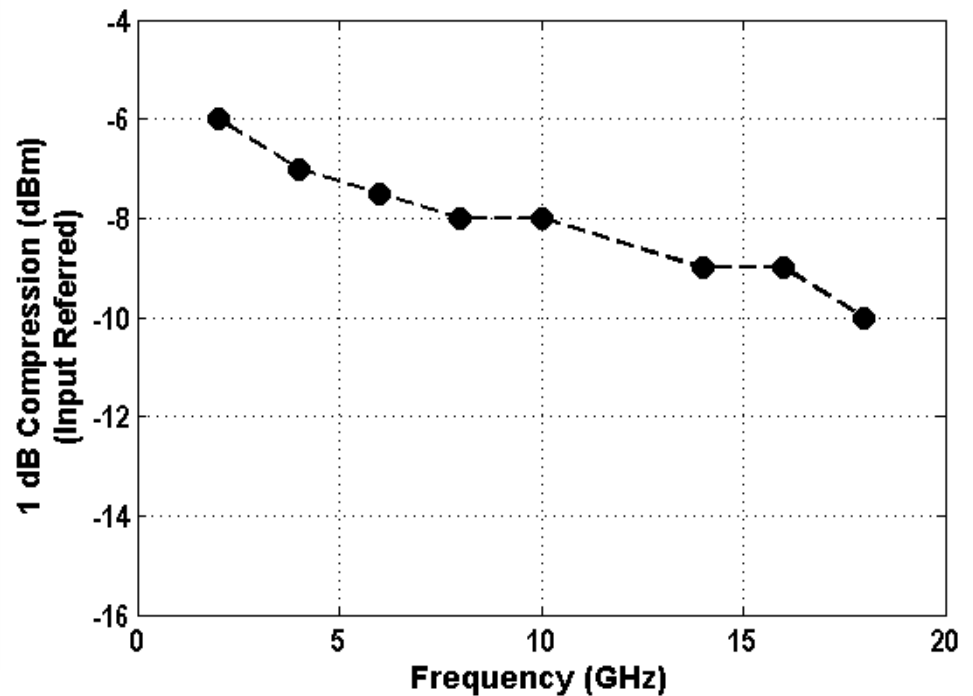
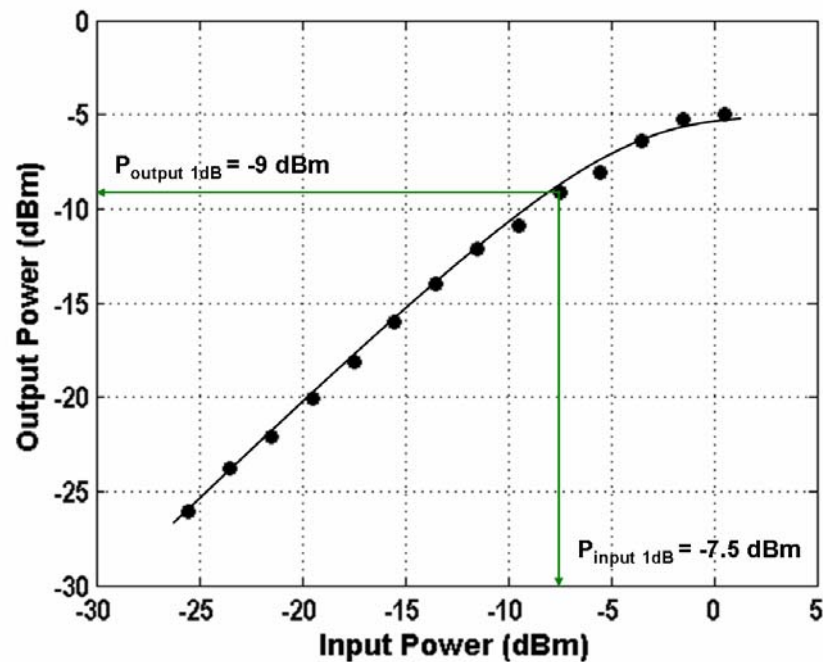
$$V_{DD} = 2.2 \text{ V}$$



6 dB was added to the S_{21} measured on a 2-port network analyzer

Measurement of g_m -Boosted Pre-amp

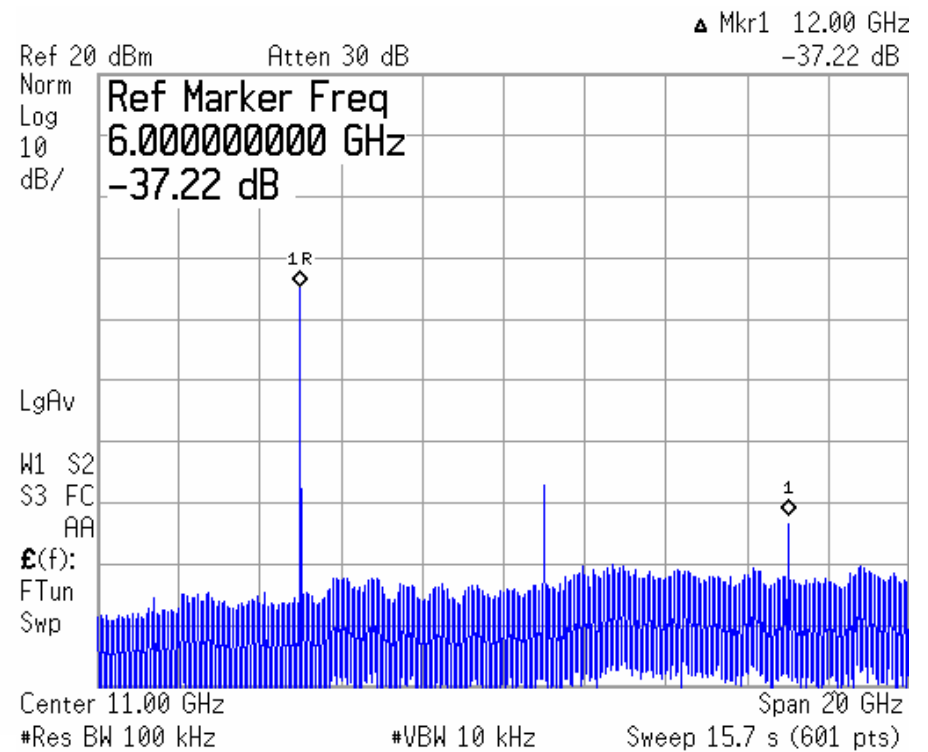
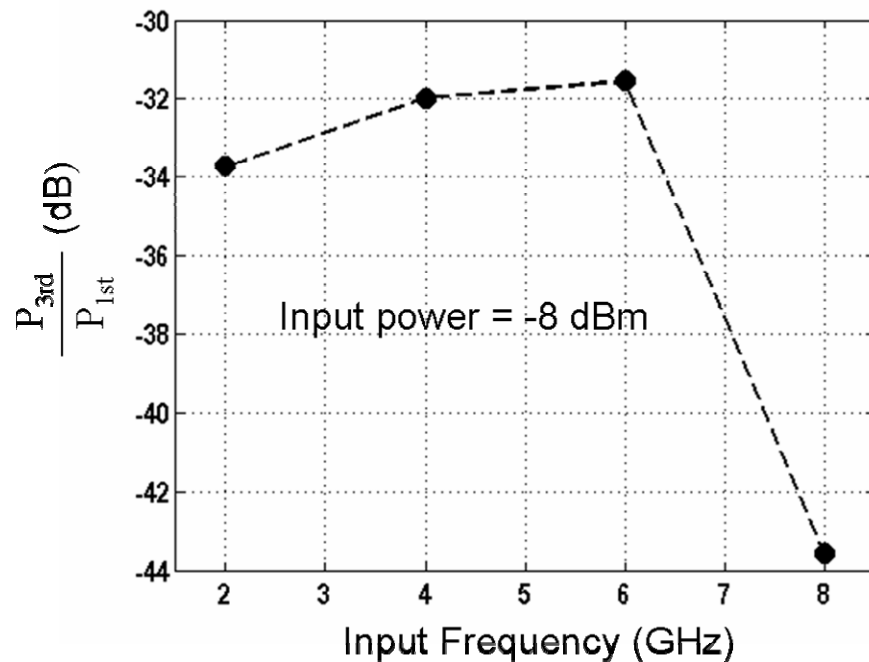
$$V_{DD} = 2.5 \text{ V}$$



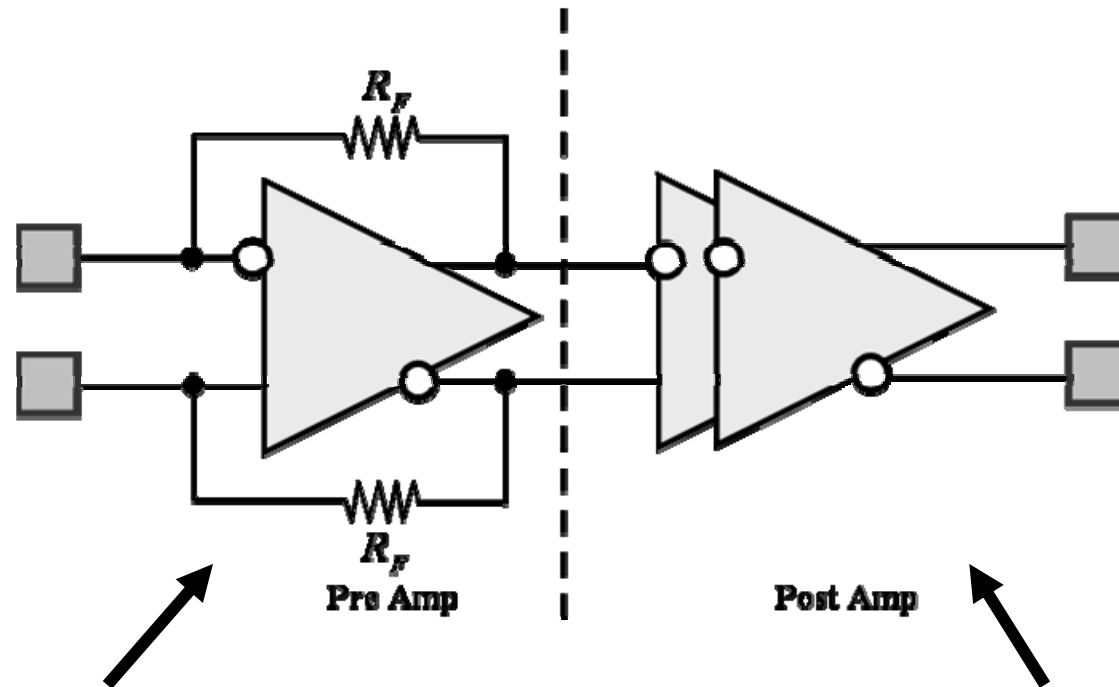
$P_{1\text{dB}}$ for 6-GHz input

Measurement of g_m -Boosted Pre-amp

$$V_{DD} = 2.5 \text{ V}$$



Full Front End Design

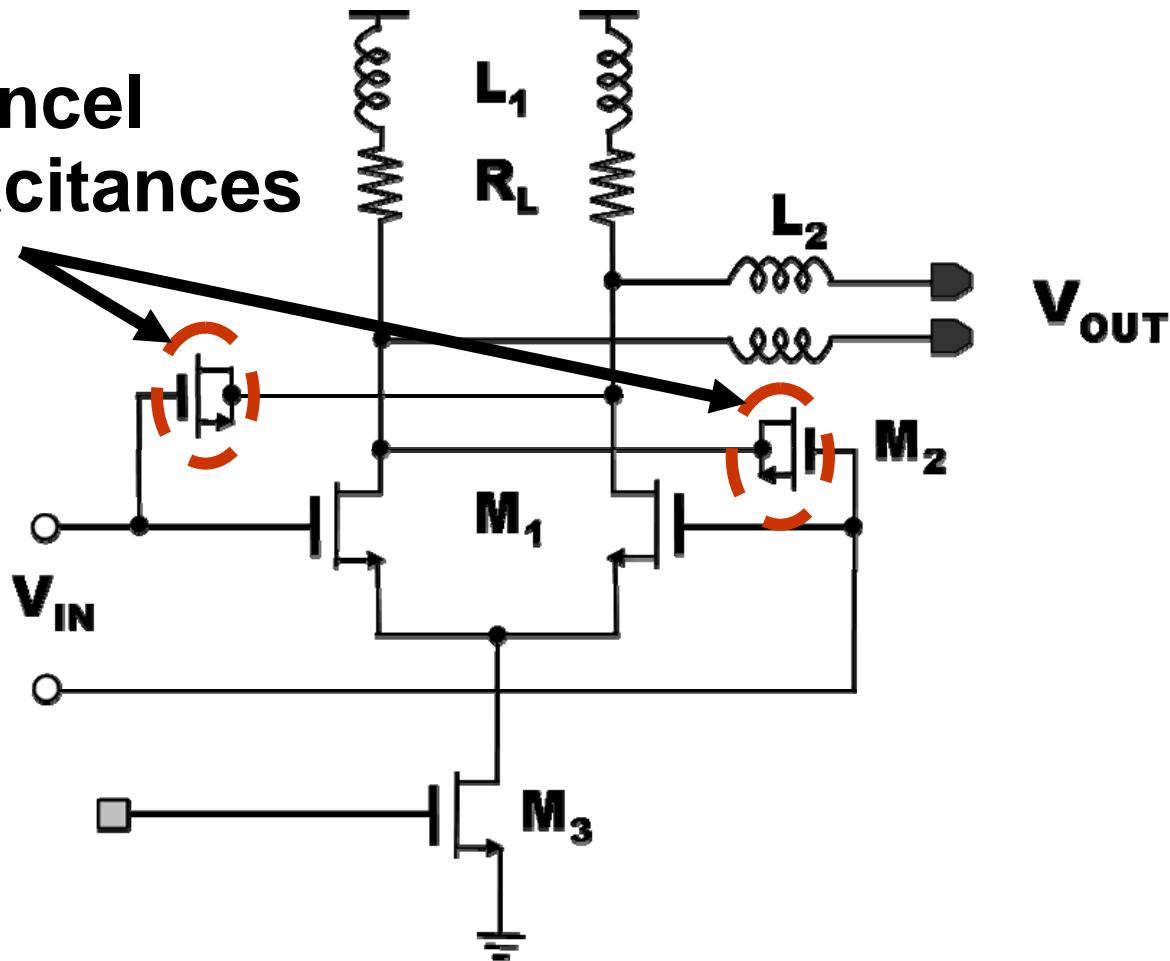


- Bandwidth > 20 GHz
- Constant group delay
- Gain > 6 dB
- 50- Ω Input Matching

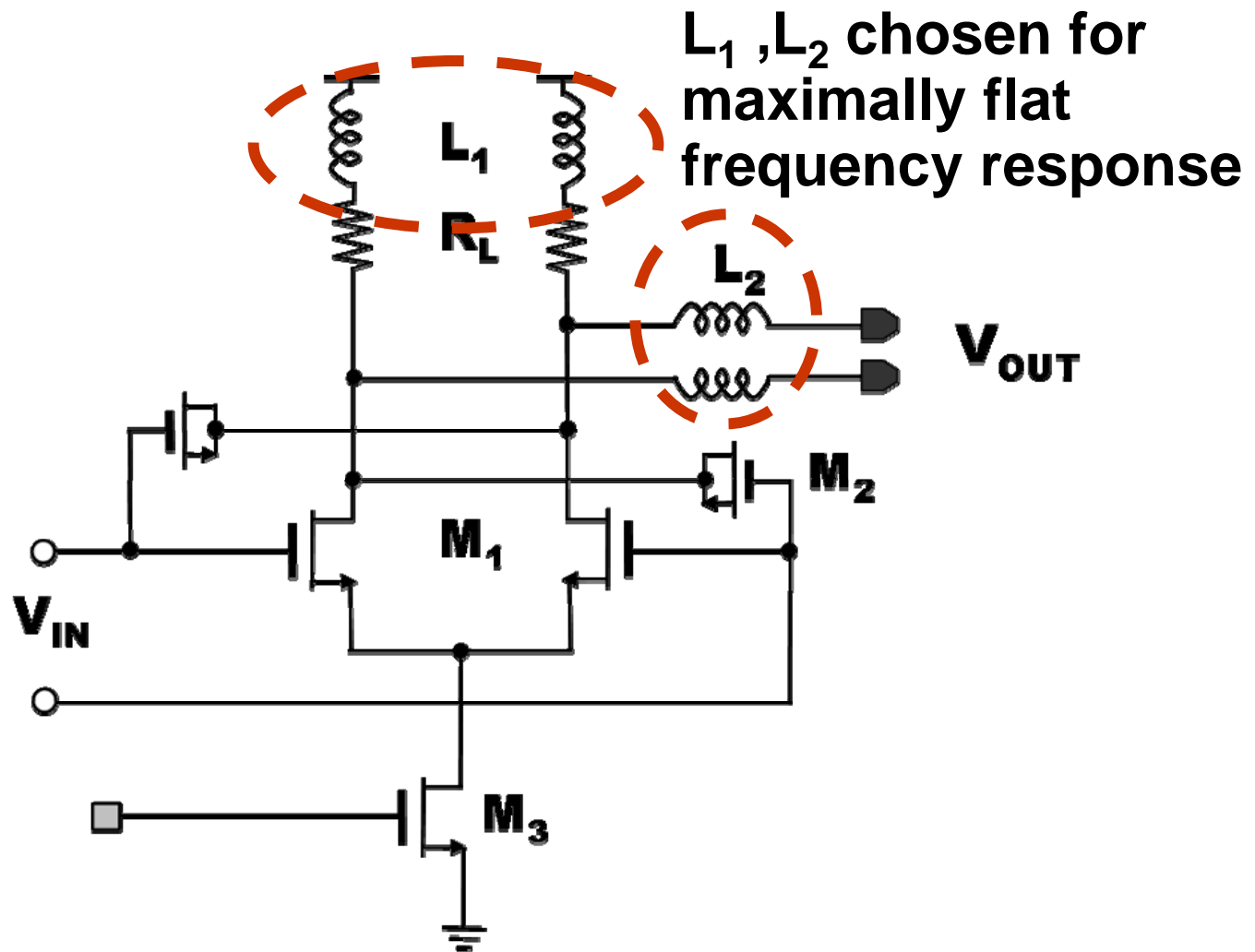
- Bandwidth > 20 GHz
- Constant group delay
- Gain > 4 dB
- 50- Ω output driver

Post-amplifier

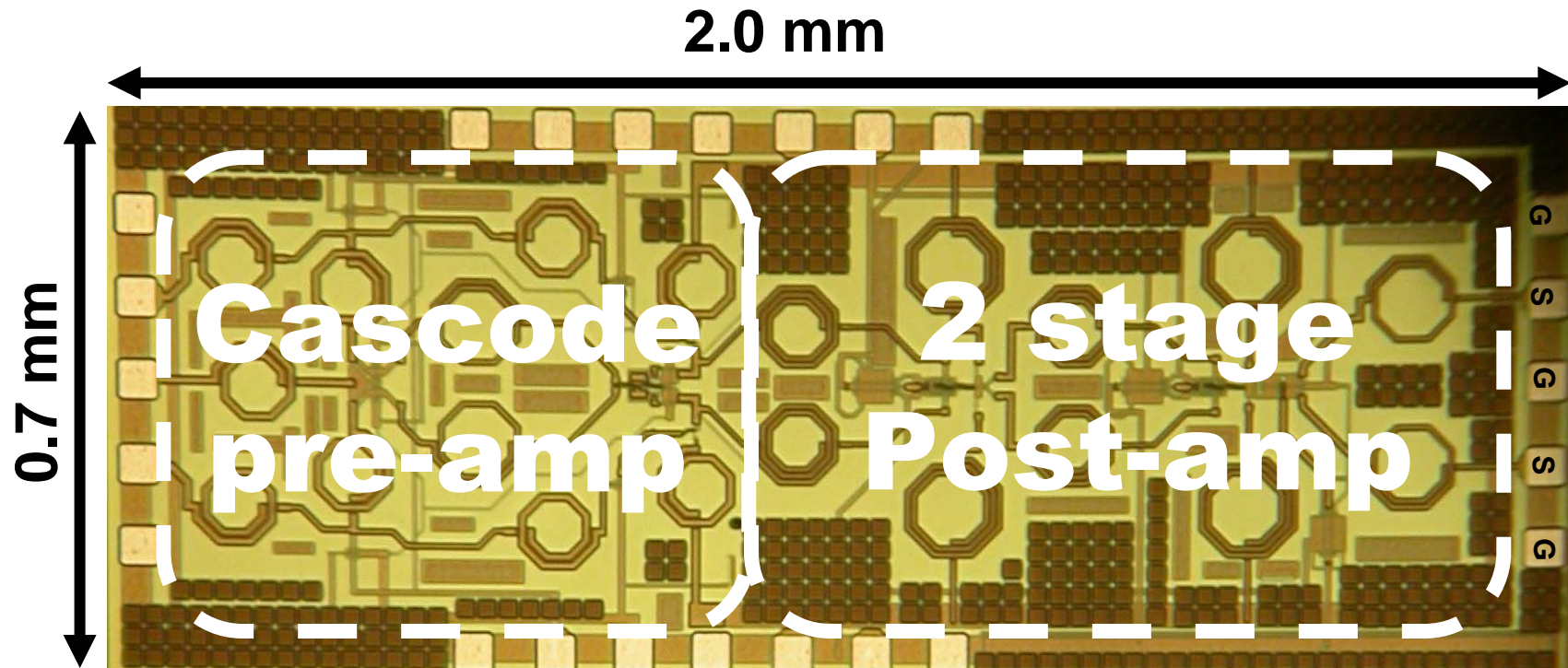
Used to cancel
Miller capacitances



Post-amplifier

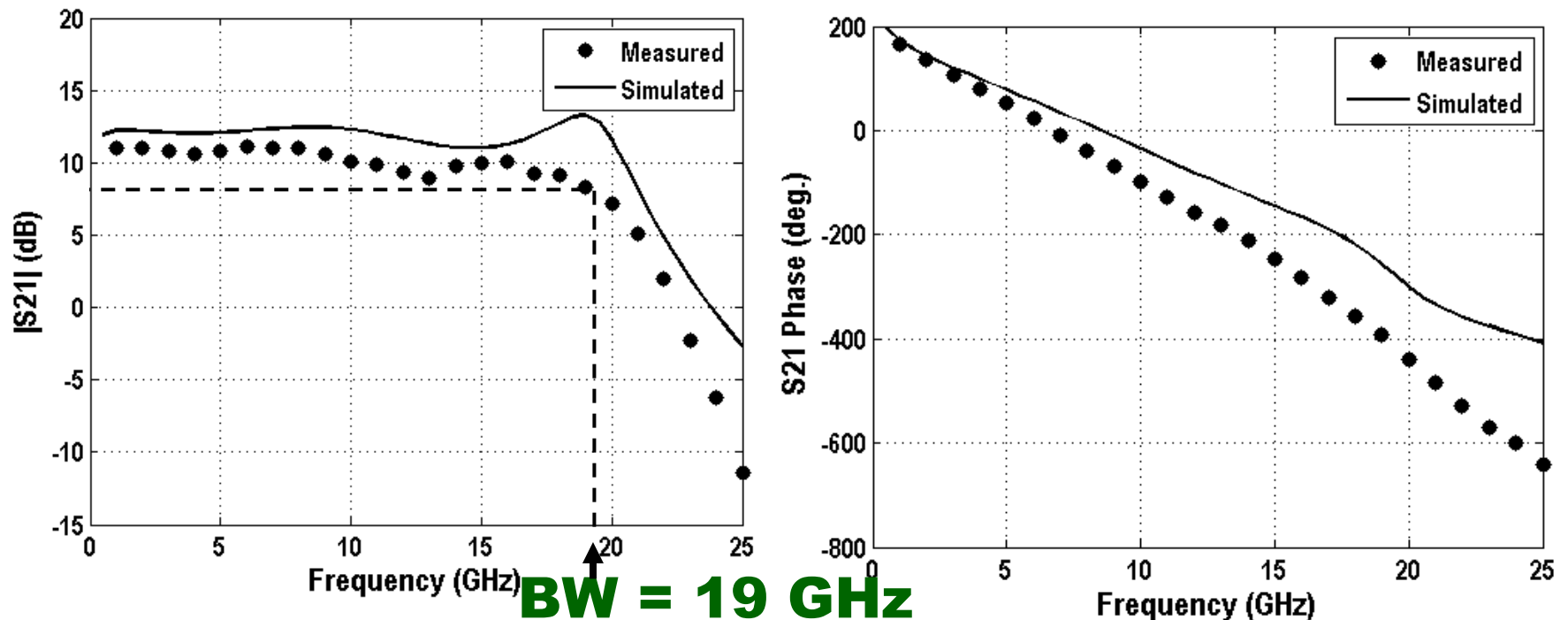


Full Front End



Measurement of Full Front End

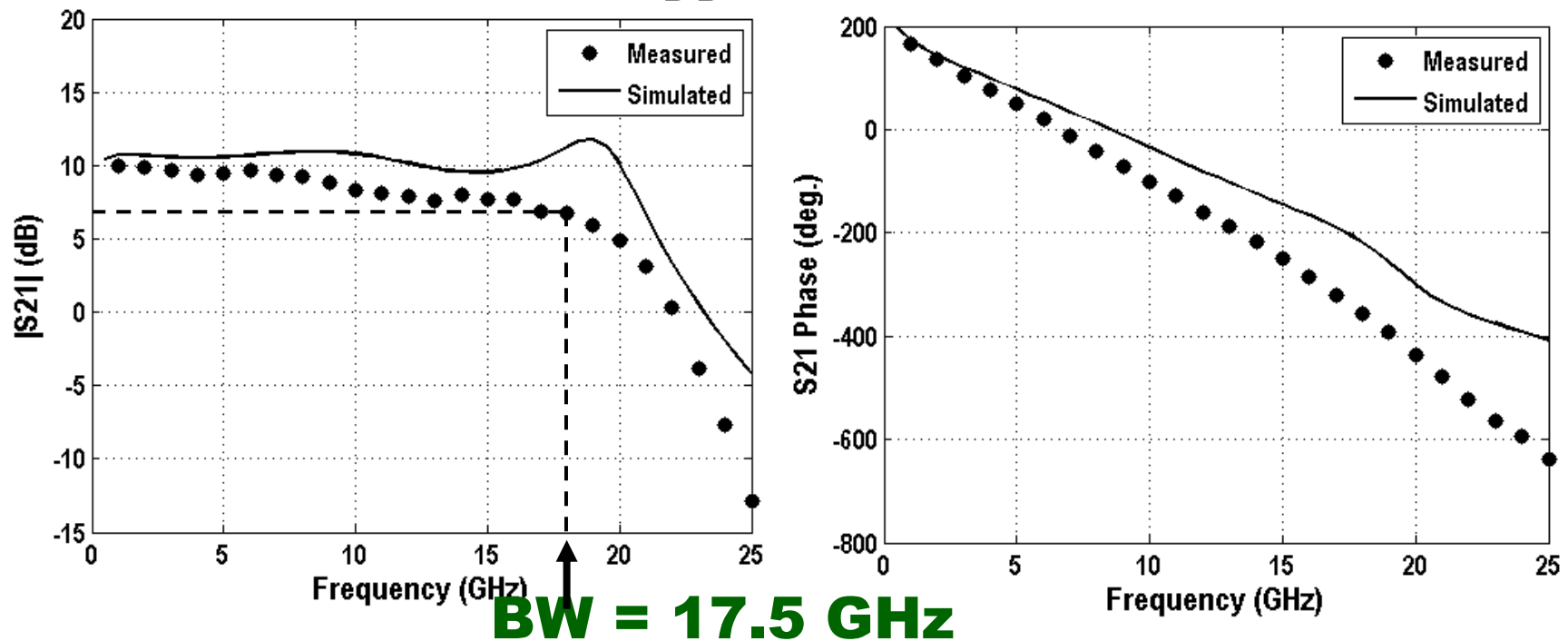
$$V_{DD} = 2.5 \text{ V}$$



6 dB was added to the S_{21} measured on a 2-port network analyzer

Measurement of Full Front End

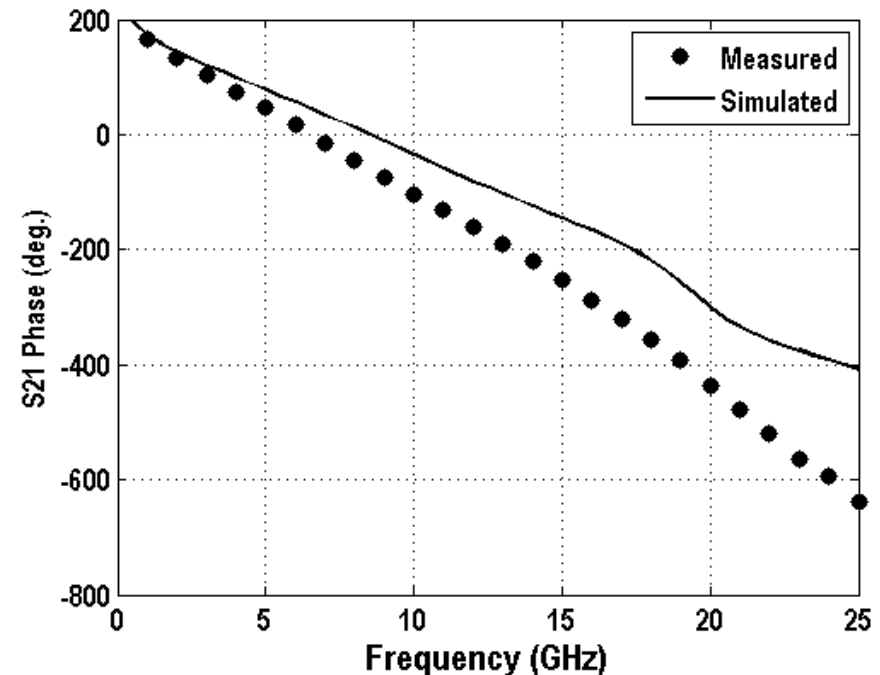
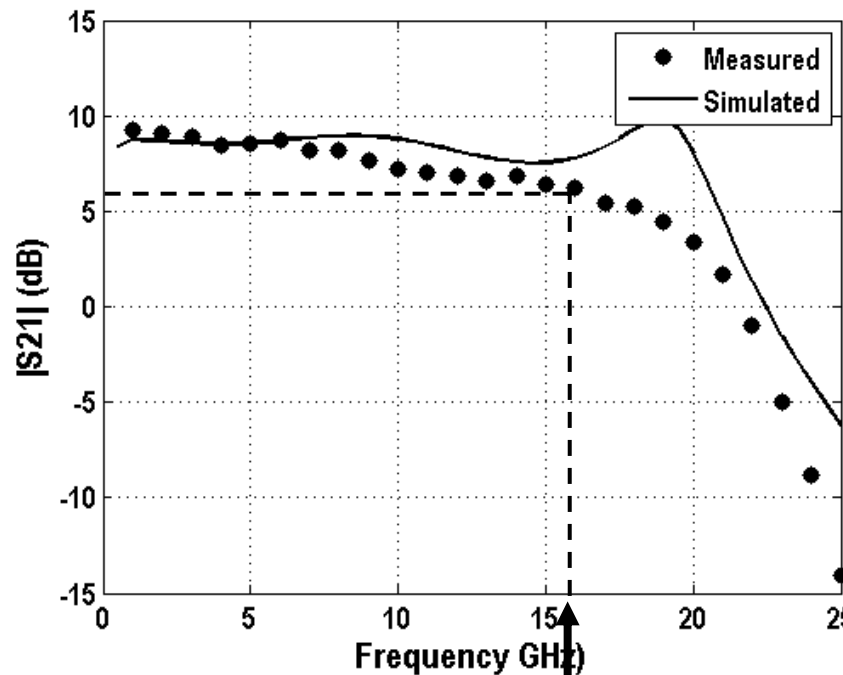
$$V_{DD} = 2.2 \text{ V}$$



6 dB was added to the S_{21} measured on a 2-port network analyzer

Measurement of Full Front End

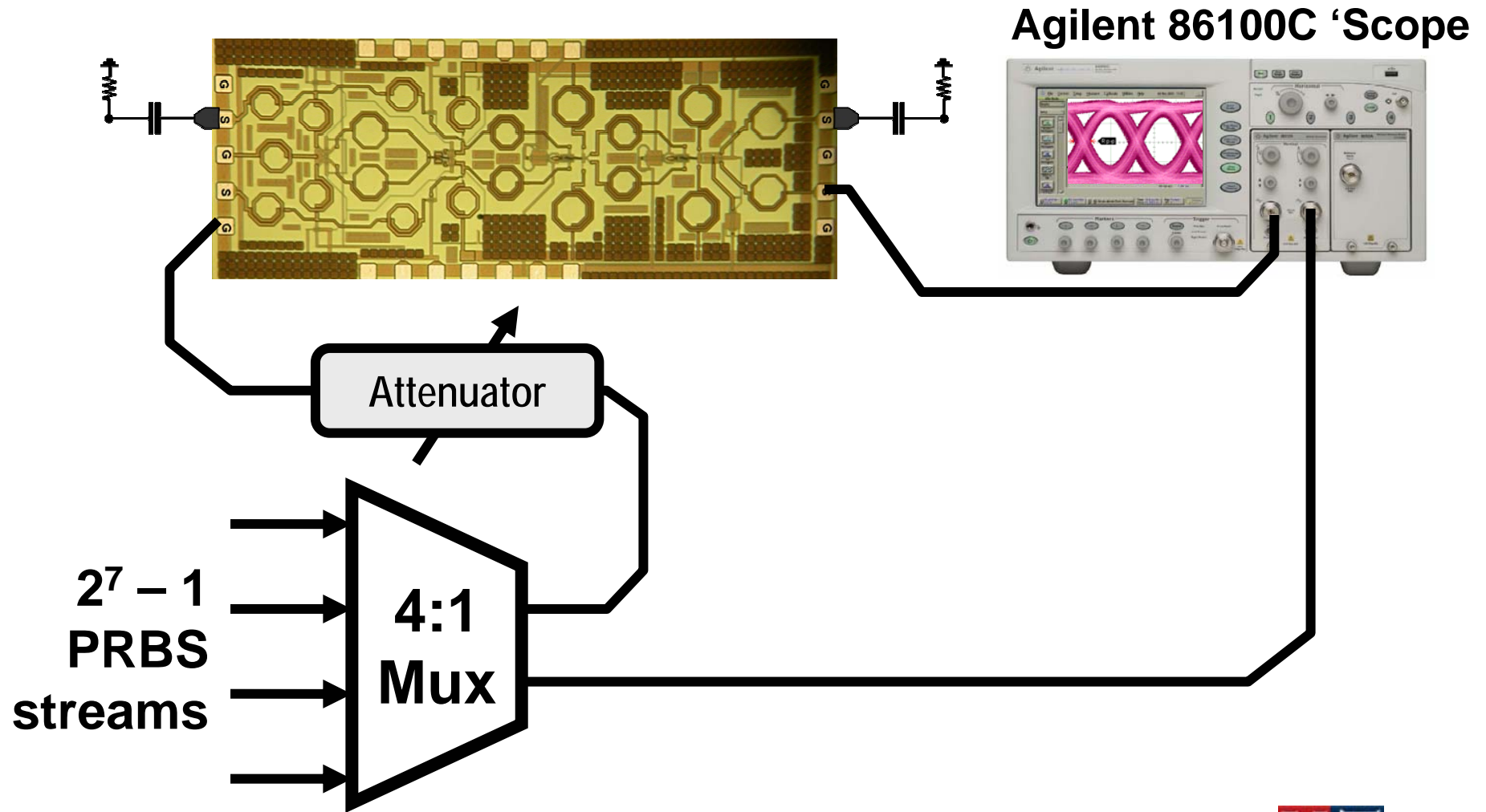
$$V_{DD} = 2.0 \text{ V}$$



BW = 16 GHz

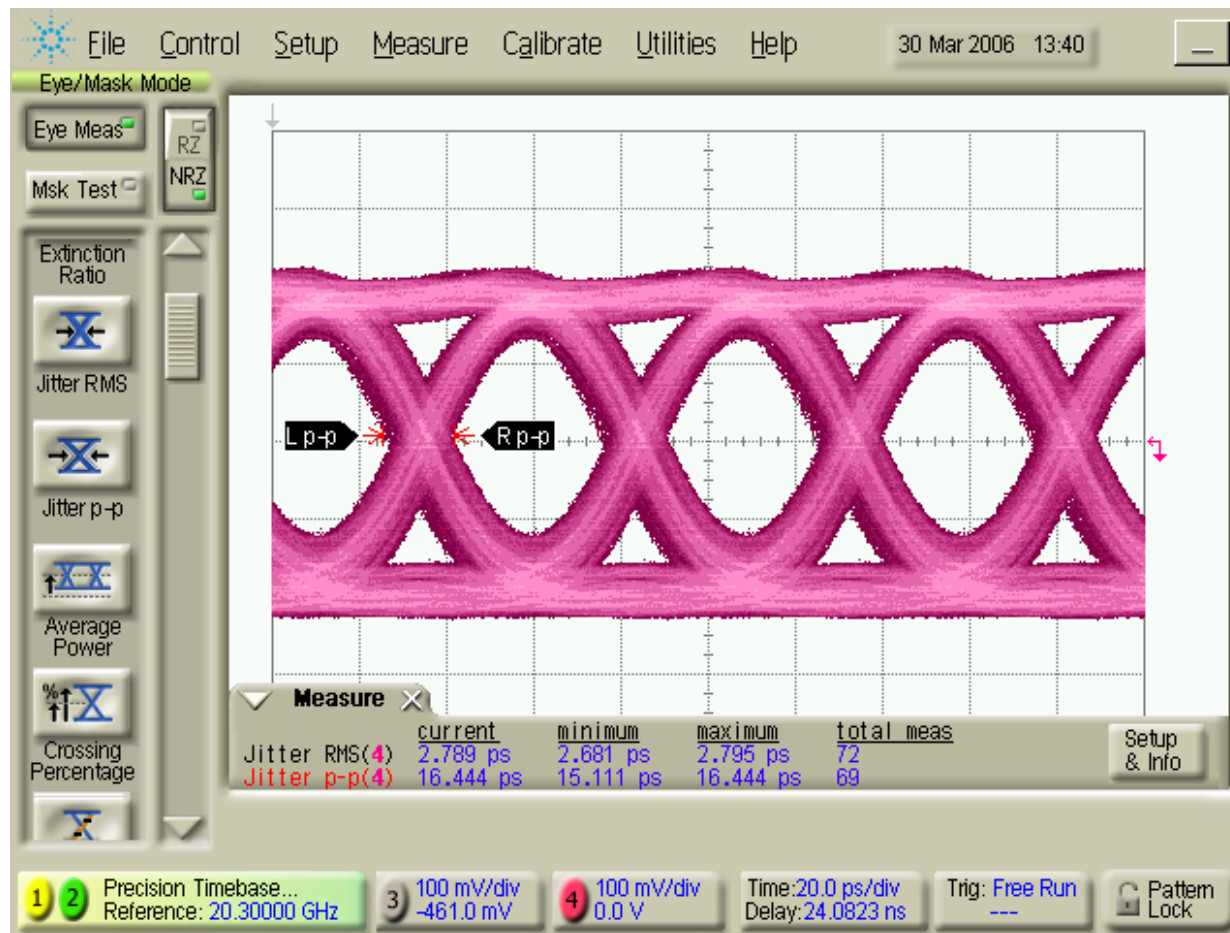
6 dB was added to the S_{21} measured on a 2-port network analyzer

Measurement Setup for Eye Diagrams



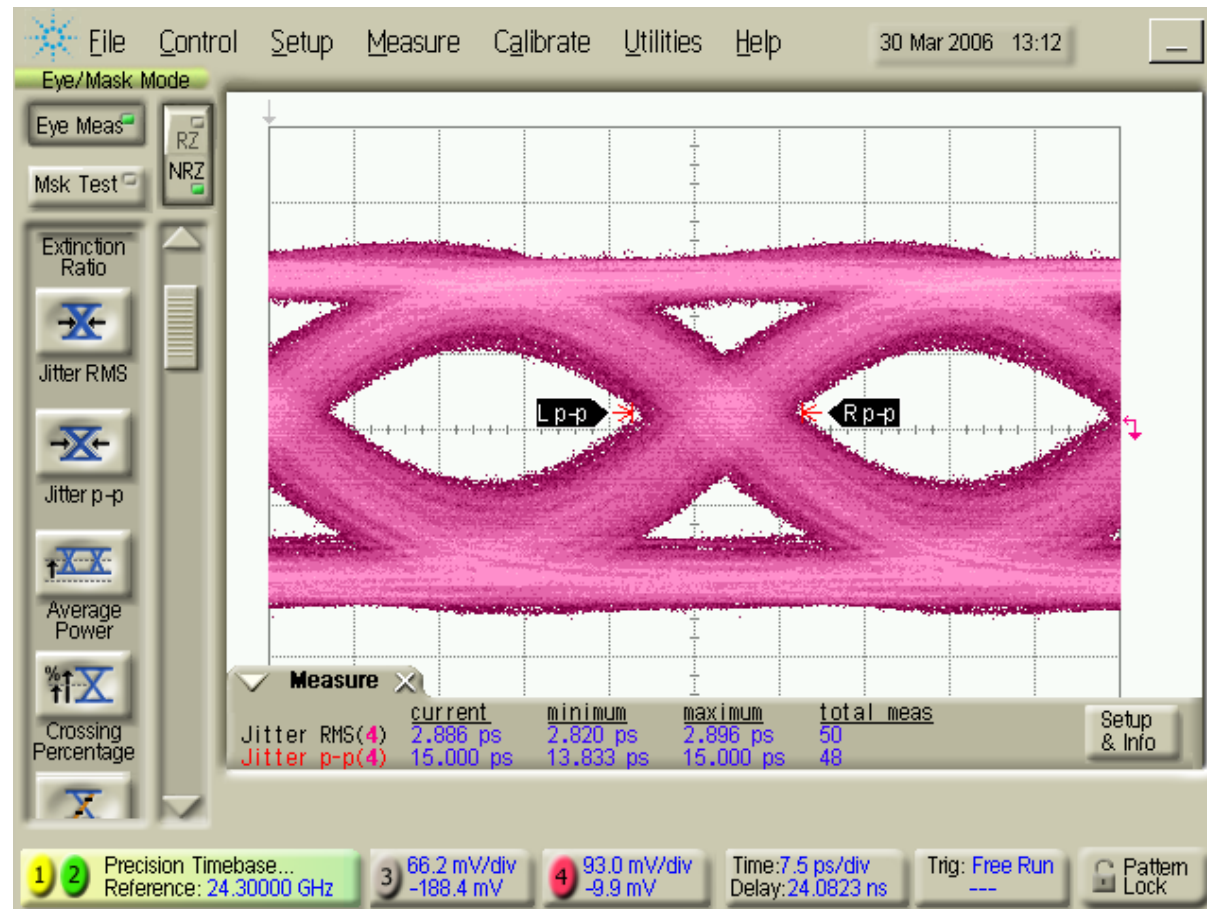
Eye Diagram Measurements

20 Gb/s, 270 mVpp input amplitude



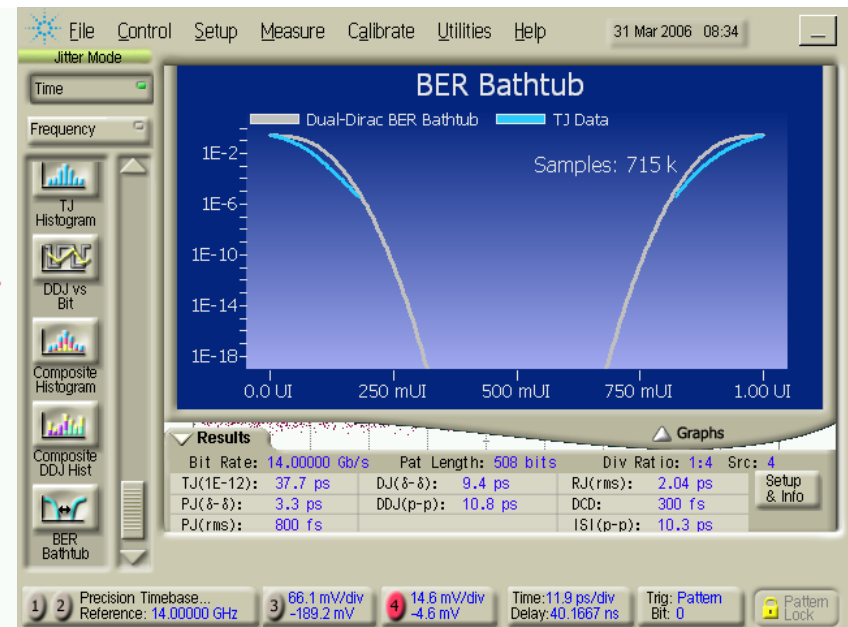
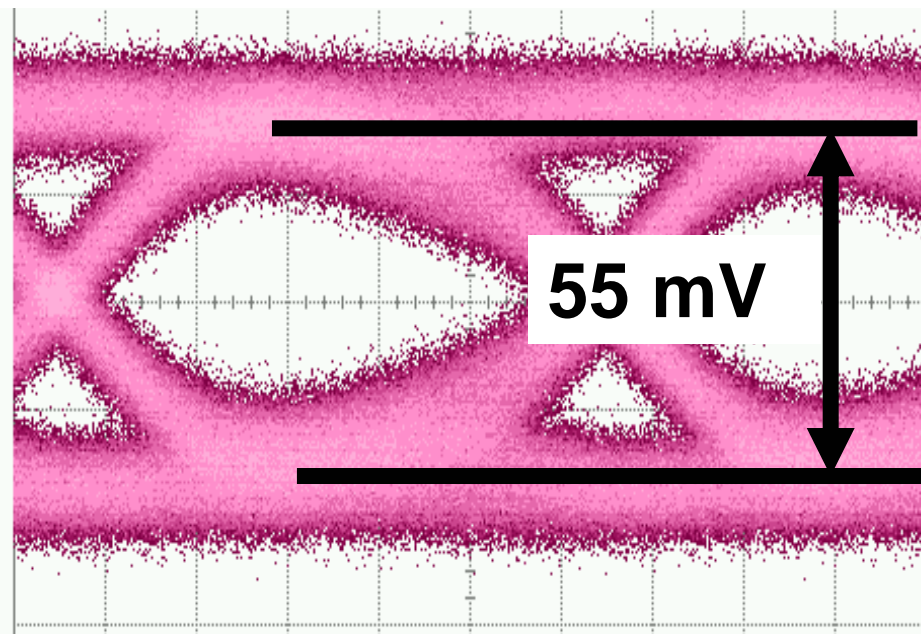
Eye Diagram Measurements

24 Gb/s, 270 mVpp input amplitude



Sensitivity Testing

14 Gb/s, 27 mVpp input amplitude



Summary

	This work	Analui'04	Bevilacqua'04
CMOS Technology	0.18 μm	0.18 μm	0.18 μm
Single ended (SE) or Differential (Diff)	Diff.	SE	SE
3 dB bandwidth (GHz)	19	9.2	7
DC $ S_{21} $ (dB)	11	—	9.3
DC $ Z_{21} $ (dB Ω)	52	54	—
Sensitivity (μW)	3.6 @ 14Gb/s	15.8 @ 10Gb/s	—
Input referred $P_{1\text{dB}}$ (dBm)	-7.5 @ 6 GHz	—	—
$P_{3\text{rd}}/P_{1\text{st}}$ (dB)	-31.8 @ 6 GHz	—	—
Power (mW)	111	137	9
Supply Voltage (V)	2.5	2.5	1.8
Area (mm^2)	1.4	.64	1.1

Conclusions

- **Passive g_m -boosting**
 - ✓ Improves the time constant at cascode node
 - ✓ Reduces Miller effect at the input node
 - ✓ Does not reduce DC gain
 - ✓ Does not introduce peaking
 - ✓ No additional power consumption
- **Pre-amplifier (only) achieves BW of 22 GHz in 0.18- μ m CMOS**
- **Front end (pre-amp + post-amp) gain > 10 dB is achieved with BW of 19 GHz**

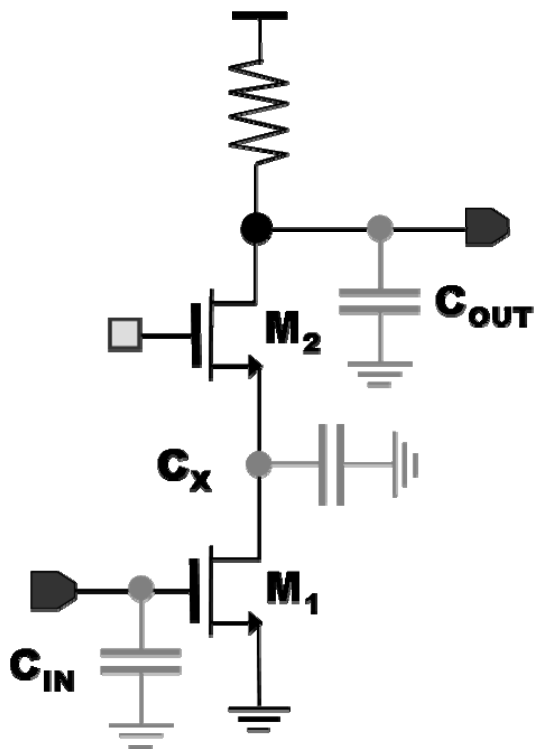
Acknowledgements

- Shahriar Shahramian
- Canadian Microelectronics Corporation
- Intel Corporation

Extras

Standard CMOS Cascode

For example, assuming
 $R_{in} = 50 \Omega$, $R_L = 150 \Omega$,
 M_1 & M_2 are $20 \times 2 \mu\text{m}$,
 $I_D = 7.5 \text{ mA}$, $C_{PAD} = 70 \text{ fF}$,
and $C_L = 40 \text{ fF}$:

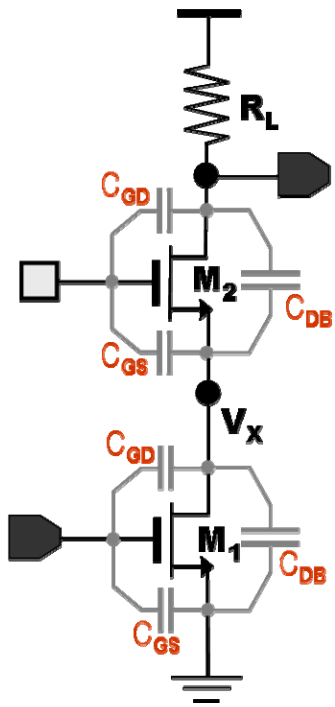


$$\tau_{out} = 15\text{pS}$$

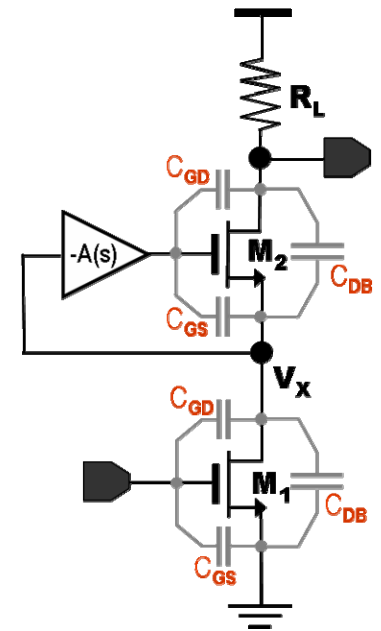
$$\tau_{cascode} = 12\text{pS}$$

$$\tau_{input} = 9\text{pS}$$

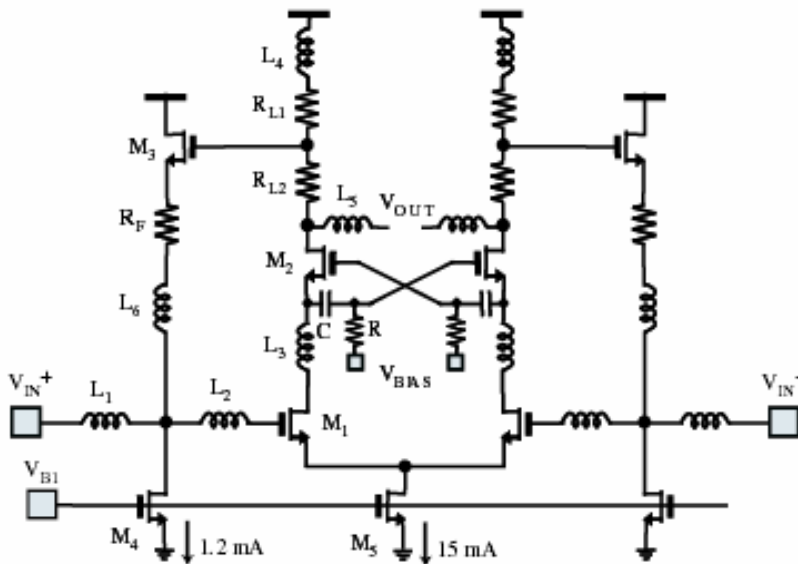
Time Constants of g_m -boosted Cascode



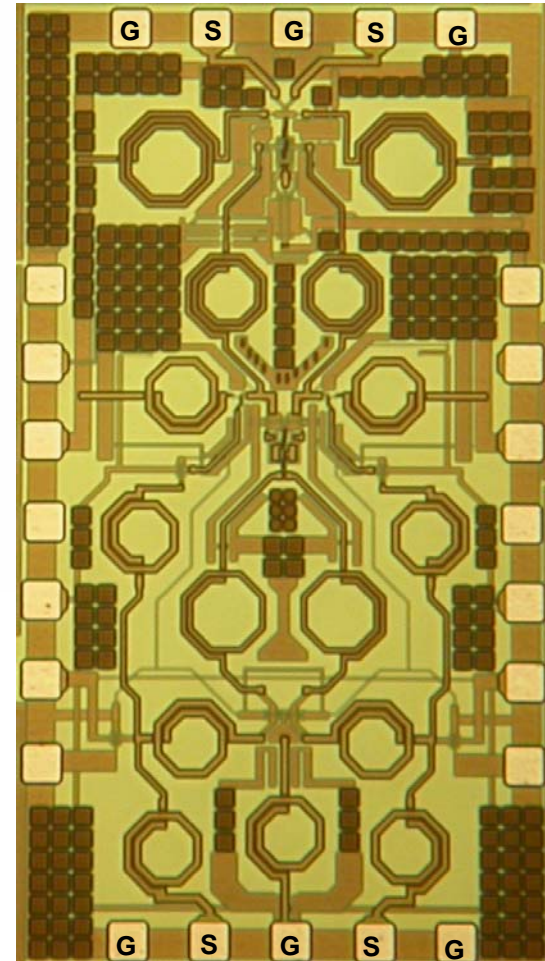
	Standard Cascode	g_m -boosted Cascode
DC Gain	$g_{m1}R_L$	$g_{m1}R_L$
τ_{Input}	$R_S[C_{GS} + 2C_{GD}]$	$R_S[C_{GS} + 1.5C_{GD}]$
τ_{CASCODE}	$\frac{C_{\text{Tot}} + 2C_{GD}}{g_{m2}}$	$\frac{.5C_{\text{Tot}} + 1.5C_{GD}}{g_{m2}}$
τ_{OUTPUT}	$R_L[C_{GD} + C_{db} + C_L]$	$R_L[C_{GD} + C_{db} + C_L]$



Differential g_m -boosted Cascode



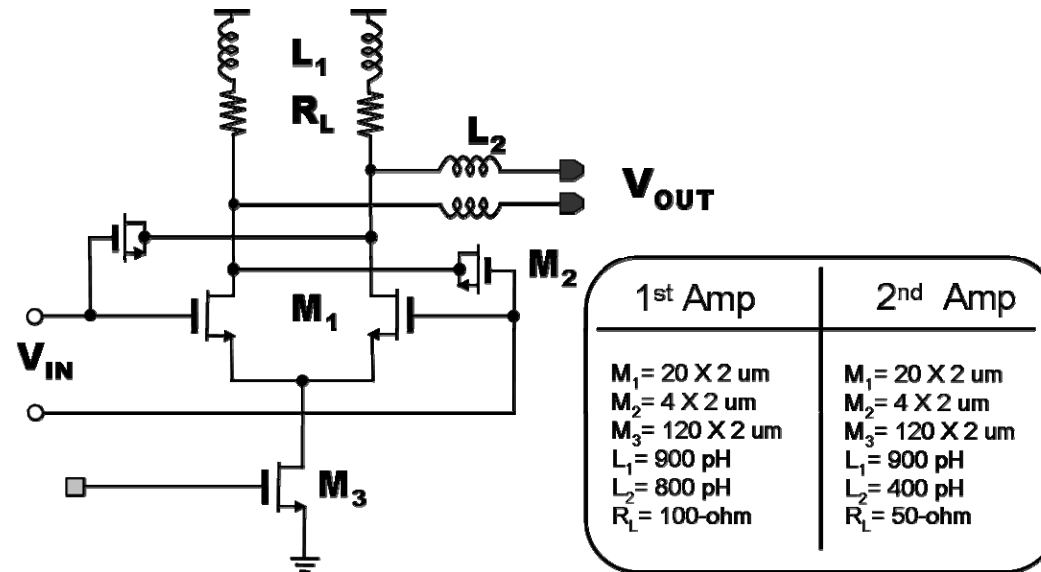
- $M_1 = 20 \times 2 \mu\text{m}$
- $M_2 = 20 \times 2 \mu\text{m}$
- $M_3 = 8 \times 2 \mu\text{m}$
- $M_4 = 7 \times 2 \mu\text{m}$
- $M_5 = 120 \times 2 \mu\text{m}$
- $R_F = 70 \text{ -ohm}$
- $R_{L1} = 100 \text{ -ohm}$
- $R_{L2} = 50 \text{ -ohm}$
- $L_1 = 200 \text{ pH}$
- $L_2 = 100 \text{ pH}$
- $L_3 = 200 \text{ pH}$
- $L_4 = 200 \text{ pH}$
- $L_5 = 800 \text{ pH}$
- $L_6 = 200 \text{ pH}$
- $C = 70 \text{ fF}$
- $R = 500 \text{ -ohm}$



g_m boosting :

- ✓ Improves Input time constant
- ✓ Improves the time constant @ cascode node
- ✓ Do not reduce DC Gain
- ✓ No additional DC power consumption

Post Amplifier Implementation



Post Amplifier

